Minnesota Technical Assistance Program

WASTE WATER REDUCTION IN METAL FINISHING AND IN CLEANING

MnTAP Intern Report—Summer 1997 Kurt Manufacturing Company Ranee A. Brunner

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Table 2, Implementation Summary for Waste Reduction Optionsfor the Automatic Division: Cost savings include water costs, sewer costs, and RO system costs. In addition SAC liability savings is listed. Each SAC unit denotes 274 gallons per day.

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Wasto	Wasto	SAC	Cost	SAG.	04-4
Deduction	Dedeed		Cost	SAC	Status
Reduction	Reduced	Reduced	Savings	Liability	
Option	(gal/yr)	(units)	(\$/yr)	Savings	
				(\$)	
Cascade in Carousel	297,480	3	892	2,850	recommended
Cascade in Crest Washer	700,150	7	1,318	6.650	recommended
Spray Rinse in Carousel	1,005,000	10	3,015	9,500	recommended
Spray Rinse Modifications in Crest Washers	876,850	9	2,753	8,550	recommended
NPDES Permit	0	9	-1200	8,550	not
RO Reject for Carousel	937,300	9	3,281	8,550	recommended

ABSTRACT

Kurt Manufacturing Company began in 1946 as a machining job shop. Since then, the company has acquired metal finishing abilities. In addition, the company offers part cleaning as a service. Both metal finishing and part cleaning require water for rinsing.

Specifically, the Machining Division and Kurt Gear Division offers metal finishing services. The Metal Finishing Line, which contains 16 five hundred gallon tanks, alone generates five million gallons of waste water annually.

Cascading rinse tanks and reducing carry-over volume will individually reduce waste water. Carry-over volume can be reduced by extending the drip-time, modifying the basket design, and by installing spray-rinsing.

Cascading rinse tanks can reduce waste water generation by 50% or 2.5 million gallons annually. In addition, an annul savings of 13 thousand dollars can be experienced. After rinse tanks are cascaded and the carryover volume is reduced, the fresh water flow rates can be optimized to minimize waste of virgin rinse water. In addition, the characterization of rinse water will lead to less cleaning of rinse tanks and ultimately less waste water. Table 1 summarizes each option that was investigated and displays the implementation status of these options.

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Waste Reduction Option	Waste Reduced (gal/yr)		Cost Savings (\$/yr)	Status
Cascade Rinse tanks				
Cascade 1	2	64,000	1,637	implemented
Cascade 2	1,9	926,000	9,992	not yet implemented
Include Tank 15 in Cascade 2	2	82,000	1,845	recommended
Cascade Tank 16 and Tank 15		0	-640	not feasible
Reduce Carry-Over Volume*	Waste	Chemicals (/yr)		
Extend Drip-Time	1950	6,814 lb 13 gal	2,513	recommended
Design New Basket	1350	3,364 lb 47 gal	1,423	recommended
Spray-Rinsing				recommended
Characterize Rinse Water	7	2,000	10,059	recommenced
Optimize Flow Rates	9:	22,000	5,716	recommended

Table 1, Waste Reduction Option Implementation Summary for the Machining Division and Kurt Gear Division: Cost savings include water costs, sewer costs, RO system costs, and chemical costs.

Additional work was done at the Automatic Division and Industrial Product Division. Waste water generation at the Automatic Division can be reduced by cascading rinse tanks, installing spray rinsing, and using reverse osmosis (RO) reject water for washing. These options were investigated to possibly reduce a service availability charge (SAC) liability. Table 2 summarizes the specific options for the Automatic Division.

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I. Background

- A. Company Description
- B. Process Description
- C. Key People

A. COMPANY DESCRIPTION

In 1946 Kurt Manufacturing Company began as a machine job shop. Since then the company has developed the capabilities to die cast, machine, test, finish, coat, deburr, and assemble. The corporate office of Kurt Manufacturing Company is located at 5280 Main St. NE in Fridley Minnesota (55421). Telephone and fax numbers are 612-572-1500 and 612-572-9878 respectively.

The company includes a total of nine divisions located at seven locations in the Minneapolis metro area, one in Nebraska, and the final location in Colorado. The general capabilities each of these divisions can best be described by the SIC codes. Fabricated metal products are represented with code 3499, which is shared by four divisions. Code 3451, shared by two facilities, denotes screw machine products. The code for aluminum die casting is 3363, and the code for electronic material is 3820. SIC Code 3544 represents special dies and tools, die sets, jigs and fixtures, and industrial molds. The final code utilized by Kurt Manufacturing company is 3842, which denotes orthopedic, prosthetic and surgical appliances, and supplies. Divisions do share capabilities, but each facility uses these abilities for different jobs. Table I-1 in displays division information, including the SIC codes, for each division.

Both the Machining Division and Kurt Gear Division are located at the Main St. address. The Machining Division is not only the largest division, but also the oldest. The division focuses on the design of anything from small screw machined parts to large fabrications and machined castings. Kurt Gear produces various types of high precision gears including spur, helical, worm, spiral, and coniflex bevel. Both divisions share metal finishing and heat treating capabilities. A combined workforce of 303 employees facilitate the needs of both divisions and SIC code 3499 represents the product lines of both divisions.

The Automatic Division, located in Coon Rapids, employs 132 people to manufacture equipment and parts for industrial use. Capabilities, denoted by SIC code 3451, of the division include automatic screw machine operation, centerless grinding, milling and secondary machining. Customers include the hydraulic, computer, military, medical, and commercial industries. The address for the Automatic Division is 1292 Northdale Blvd. NW, Coon Rapids (55448). The telephone and fax numbers are 612-572-4488 and 612-786-6336 respectively.

The Industrial Product Division located at 1325 Quincy St. NE in Minneapolis (55413) employs 94 people to fulfill specific needs of industry. The workholding product line includes power draw bars, high precision chucks, tooling blocks, and specialty vise jaws. These products are represented by SIC code 3544. The division telephone number is 612-572-4424 (800-328-2565) and the fax number is 612-623-3902.

The remaining sections of the company include the Pueblo Division, the Lyman Division, the Theradyne Division, the Kurt Die Casting Division, and finally the Electronic Division. The Pueblo Division, in Colorado, possesses Class 100 clean room facilities. These facilities allow the division to fulfill the machining needs of the computer industry. The Lyman Division, in Nebraska, maintains automatic screw machining capabilities, grinding abilities, and cutter operation capabilities. The Theradyne Division, in Jordan, manufactures products such as wheelchairs and truck bumpers. The remaining divisions, Kurt Die Casting and Electronic, are both located in Fridley. The Kurt Die Casting Division provides customers with trim dies and die maintenance. Finally, the Electronic Division increases the capabilities of Kurt Check Gaging Systems.

Each of the divisions will benefit from the reduction of water usage. Although, this project focuses on the specific needs at the Main St. address and at the Automatic Division. Some additional work has been done at the Industrial Product Division.

Table I-1, Division Locations, Contact Information, Number of Employees, and SIC Codes: Kurt Manufacturing Company is comprised of nine individual divisions. Seven of the divisions are located in the Minneapolis area, and the remaining divisions are located in Nebraska and Colorado.

Division	LLA				
	Address	Telephone	Fax	People	SIC Code
Corporate Headquarters	5280 Main St. NE	(612)572-1500	(612)572-9878	54	
Machining and	5280 Main St. NE	(612)572-1500	(610)570.0070		
Kurt Gear	Fridley, MN 55421	(012)072-1000	(012)572-9878	303	3499
Automatic	Automatic 1292 Northdale Blvd. NW Coon Rapids, MN 55448		(612)572-0801	132	3451
Industrial Product	1325 Quincy St. NE Minneapolis, MN 55413	(612)572-4424 (800)328-2565	(612)623-3902	94	3544
Pueblo	350 Keeler Pkwy. Pueblo, CO 81001	(719)948-4477	(719)948-3749	100	3499
Lyman	Jeffers and O St. Lyman, NE 69352	(308)787-1211	(308)787-1281	103	3451
Theradyne	395 Ervin Industrial Blvd. Jordan, MN 55352	(612)502-9190	(612)492-3443	92	3842
Kurt Die Casting	7585 Highway 65 NE Fridley, MN 55432	(612)572-4650	(612)786-6336	155	3363
Electronics	7585 Highway 65 NE Fridley, MN 55432	(612)572-4597 (800)343-9884	(612)784-6055	17	3820

SIC Code Descriptions:

3499—fabricated metal products

3451—screw machine products

3544—special dies and tools, die sets, jigs and fixtures, and industrial molds

3842—orthopedic, prosthetic, and surgical appliances and supplies

3363—aluminum die casting

3820—electronic material

B. PROCESS DESCRIPTIONS

Waste water reduction in the Metal Finishing Line at the Main St. plant was the primary focus of the project. An additional area of waste water concern was the overall plant consumption at the Automatic Division. Finally, some time was spent analyzing the • metal finishing line at the Industrial Product Division.

1. Machining Division and Kurt Gear Division

The Metal Finishing Line at the Main St. alone generates six million gallons of waste water annually. As shown in figure I-1, eight rinse tanks and eight process tanks form the Metal Finishing Line. A detailed diagram is included as figure V-3 in appendix C. Each tank in the line has a 500 gallon capacity. Figure I-1 also shows the annual waste generation for each tank.

Residue metals and surfactants from a preliminary deburring process are cleaned from the parts during metal finishing. Water soluble coolant films, from machining, need washed from the parts.

An automatic hoist moves baskets, which are filled with parts, from one tank to the next. Tank 1 in the line contains an alkaline, which is used to clean the parts before any further finishing. An acid cleaner, which is currently not in use, is contained in tank 2. Tank 4 contains a basic etchant, which is used for further cleaning of aluminum parts. Aluminum parts are cleaned further in tank 7 with an acidic deoxidizer. Die cast aluminum is again cleaned with a nitric acid cleaner in tank 10. To protect against corrosion, the parts can be treated with chromic acid conversion coatings in either tank 13 or tank 14. Tank 13 contains a clear iridite, while tank 14 contains a yellow iridite. The clear iridite coating is chosen when the parts will not be painted and the yellow finish is applied if the parts are

	•	and the second
_K 16	Hot Rinse: 130°F to 140°F Ogel 18M gal/year (sewer) KO Dead R	, MM &
R 15	Iridite Rinse Ko 70,5 jph 300M gal/year (sewer)	
14 old	Yellow Iridite: 90°F 500 gal/year (hazardous)	300 500
13 cold	Clear Iridite: 90°F 500 gal/year (hazardous)	2,500 900 1000
12 R	Rinse R0 2.5MM gal/year (sewer)	18 913
11 R	Acid Rinse Tap Water 2115 gph 900M gal/year (sewer) 35gpm	300 100
10 esta	Nitric Acid Cleaner 500 gal/year (hazardous)	6700
9 Not	Passivate: 120°F to 125°F 500 gal/year (hazardous)	
8	Deoxidizer Rinse Ro 5409ph 1MM gal/year (sewer) 9 gpm	
7 cold	Deoxidizer: 90°F 6M gal/year (hazardous)	
R 6	Rinse \mathcal{R}_{0} 18M gal/year (sewer) \mathcal{O} $\mathcal{T}_{0}^{\mathcal{R}}$	
r 5 🗲	Etchant Rinse Rb 50 gph 918M gal/year (sewer)	Figure I-1, Original Schematic of the
4 hot	Etchant: 100°F to 160°F 6M gal/year (sewer)	Metal Finishing Line at the Main St. Plant: The approximate
R 3	Alkaline Rinse NV Or gan 300M gal/year (sewer) Jann	amount of waste generated annually is included. The tank
2	Acid Cleaner (not in use)	temperature if not noted.
1 hot	Alkaline Cleaner: 150°F to 180°F 4.5M gal/year (sewer)	

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to be painted. Steel can also be finished in this line, with the passivate solution in tank 9.

Reverse osmosis (RO) water is fed to each of the rinse tanks except for tank 11 which is fed with tap water. Tanks 6 and 5 are operated in countercurrent flow, while the remaining tanks each have fresh water feed. During operation the parts may be rinsed twice in separate dip-rinse tanks. This double rinsing occurs after the etchant process (tank 4), after the acid tanks (tank 9 or tank 10), and after iridite finishing (tank 13 or tank 14). Tank 9 is used only to passivate stainless steel and tank 10 is used only to clean die cast aluminum. No process utilizes both Tank 9 and Tank 10. The final rinse tank (tank 16) is a hot water rinse. Based on operator observation, the combination of the cold and hot water rinses following the iridite tanks allows for a smooth iridite finish on the parts.

Multiple processes may be operated in the Metal Finishing Line throughout any work day. The number of process tanks used depends on metal type and customer requests. Hence, the number of rinse tanks used depends on the process tanks used. Primary operation occurs between 6:00 a.m. and 4:00 p.m., Monday through Friday. Additional operation does occur during the evenings between 4:00 p.m. and 2:30 a.m. Metal finishing is rarely completed during the weekend.

After the parts are metal finished, they are shipped either to the customer or for further processing. Additional painting can be accomplished within the plant or by another source while, anodizing must be done by another company.

2. Automatic Division

The Automatic Division faces a Service Availability Charge (SAC) liability. The SAC baseline is defined as the maximum amount of water that can be disposed of through a sanitary sewer in one working day. The baseline is specified by a unit, which is 274 gallons. The current SAC

baseline is 43 units per day (11,782 gallons per day), but the facility operates at 81 units per day (22,194 gallons per day). In general, a facility is charged \$950 per unit for any excess sewer disposal. Therefore the Automatic Division must reduce waster water disposal by 38 units (10,412 gallons per day) before the \$36,100 SAC liability will be reduced. The main areas of waste water generation include the RO system and three washer systems. Possibilities for waste water reduction in each of these areas will be discussed.

In addition to the SAC liability, the facility has been experiencing problems with part quality. Specifically, the washer systems have not been adequately cleaning the spacers. Therefore the primary concern of the plant is correct this cleanliness problem. The threat of lost profit from poor part quality is a greater threat than the Sac liability. Hence changes that can reduce the SAC liability may be neglected. Although, these changes can be made for future cost reduction and for future waste water reduction.

Before the spacers are cleaned, they are placed in a grinding system. After grinding the spacers move through two separate washing systems. The first system, Carousel Washer System, initially washes the spacers with an alkaline cleaner and a deoxidizer. From the Carousel Washer System the rack of spacers is manually moved to one of two Crest Washer Systems. Each of the Crest Washer Systems perform a final cleaning of the spacers with an alcohol blend. After proper cleaning the parts are immediately packaged for the customer. Although some of the spacers may be sampled throughout the day for cleanliness quality.

a. Carousel Washer System

The primary use of the Carousel Washer System is to perform preliminary cleaning of parts. The parts move through the system on racks, which are moved from one tank to the next by an automatic arm. The system contains 11 tanks each with a 209 gallon capacity as shown in Figure I-2. Annual waste generation for each tank is included in the figure.

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Tank	Description	Waste Generation	Comments
1	Alkaline Cleaner Alkalume 143	11M gal/year	
2	Alkaline Rinse	1.0MM gal/year	
3	Alkaline Cleaner Alkalume 143	11M gal/year	
4	Hot Alkaline Rinse	457M gal/year	
5	Hot Rinse	11M gal/year	Waste Feeds 4
6	Rinse	308M gal/year	
7	Rinse	11M gal/year	Waste Feeds 6
8	Deoxidizer Alkalume	2.5M gal/year	
9	Hot Deoxidizer Rinse	0 gal/year	Spray Rinse
10	Hot Rinse	1.0MM gal/year	Waste Feeds 9
11	Hot RO Rinse	4.1MM gal/year	

Figure I-2, Schematic of the Carousel Washer at the Automatic Division: Only one tank (tank 8) contains a hazardous material. The remaining tanks can be disposed of to the sewer without any pre-treatment. Tank 8 is cleaned monthly and the remaining tanks are cleaned weekly. Parts are first cleaned with an alkaline cleaner in tank 1. The parts are then rinsed in tank 2 before being cleaned in tank 3 with the same alkaline cleaner. The parts then proceed through a series of four rinses in tanks 4, 5, 6, and 7. After the parts are thoroughly rinsed, they are cleaned with a deoxidizer in tank 8. Tank 9 is a spray rinse, which uses water from Tank 10, to rinses the parts before they are dip-rinsed in tanks 10 and 11. Water is also conserved by the use of two cascades, tanks 4 and 5, and tanks 6 and 7. Each of the tanks is cleaned weekly except tank 8 which is cleaned monthly. All tanks use well water except for tank 11 which uses RO water. After the parts are cleaned in the Carousel Washer System, they are moved to one of the Crest Washer Systems for additional cleaning.

b. Crest Washer Systems

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Each of the two Crest Washer Systems utilize similar steps to generate clean parts. In each system the parts are rinsed initially rinsed in an ethoxylated alcohol blend. Then the parts enter a series of rinsing and drying steps.

Figure I-3 shows a schematic of the Old Crest Washer Model K#1047. This washer system contains a total of four tanks. Tank O1 contains the ethoxylated alcohol blend. The remaining tanks are used for rinsing. Tank O2 is a hot spray rinse, tank O3 is a dip rinse, and tank O4 is a high pressure spray rinse. Each of the tanks uses RC water and has a 25 gallon capacity.

	1	2	3	4	
Tank	Description		Waste Gener	ation	Comments
1	Ethoxylated Alcoho	ol	18M gal/ye	ear	
2	Hot Alcohol RO Rin	se	114M gal/y	vear	Spray Rir se
3	RO kinse		249M gal/y	rear	
4	High Pressure RO Ri	nse	114M gal/y	ear	Spray Rinse

Figure I-3, Schematic of the Old Crest Washer Model K#1047: The entire system uses RO water and the tanks have a 25 gallon capacity. All waste water can be disposed of through the sewer

The New Crest Washer Model K#2424, which contains six tanks, is depicted in figure I-4. Each of the tanks has a 48 gallon capacity. The first two tanks, N1 and N2, contain ethoxylated alcohol blends. Tank N3 is a spray rinse followed by rinse tanks, N4 and N5. Tank N6 is a spray rinse combined with a hot air dry. These six tanks also use RO water.

1	2	3	4	5	6

Tank	Description	Annual Waste Generation	Comments
1	Ethoxylated Alcohol	34M gal	
2	Ethoxylated Alcohol	34M gal	
3	Alcohol DI Rinse	114M gal	Spray Rinse
4	RO Rinse	265M gal	
5	RO Rinse	233M gal	
6	RO Rinse	114M gal	Spray Rinse and Hot Air
	·		Dry

a GG 12 Alaget

Figure I-4, Schematic of the New Crest Washer Model K#2424: The entire system uses RO water and the tanks have a 48 gallon capacity. All waste water can be disposed of through the sewer

c. RO System

Essentially, the RO system is a membrane system that removes metals from tap water. Debris and large dirt particles are first removed from the water through mechanical separation. The water then passes through a membrane filtration system where calcium, magnesium, iron, and additional metals are removed from the water. The resistivity of the water is tested before it is discharged to the holding tank. About one-third of the water fed to the RO system is passed to the sewer as a reject stream.

Changes can be made to each of the systems to reduce the amount of water used. Immediate changes to the washer systems can reduce SAC costs significantly. Although these changes may not be feasible for product quality. Alterations can also be made to the system that will improve rinsing quality and effectiveness. These changes will reduce overall water consumption in the long-run, but may not reduce the SAC liability. Ultimately operating costs from water use and discharge can be decreased by altering the systems for improved rinsing quality. Operation occurs 24 hours per weekday and for eight hours each weekend day. The system is shut down each Monday for about six hours for cleaning. Hence the cleaning process is operated for 130 hours per week.

3. Industrial Products Division

A metal finishing line is currently not in use. Operation requires generous amounts of hazardous material disposal. The type of part does not allow for proper drainage of chromic acid. Hence an excess amount of chromic acid is carried from one tank to the next.

The process is similar to the one at the Main St. Plant where the parts are cleaned with an alkaline solution and an etchant. After cleaning the parts proceed to a chromic acid iridite line, where a conversion coating is applied. The problem occurs with the iridite half of the line, when the parts hold generous amounts of chromic acid. Hence, the first of three rinse tanks is quickly contaminated with chromic acid and must be disposed of as a hazardous material. Preliminary assessment of the problem was done and brief suggestions were made.

C. KEY PEOPLE

Many people contributed to the success of waste water reduction at Kurt Manufacturing Company. Table II-2 lists primary contributors and contact information and appendix E contains a full listing of resources contacts for the project.

Name	Position	Company	Telephone
Karl DeWahl	Senior Engineer	MnTAP	(612)627-1904
Roger Knaus	Operator	Kurt Manufacturing 7	63 (612) 572-4565
Dave Muncy	Operator	Kurt Manufacturing 7	3 (612) 572-1500
Jim Sjoselius	EHS Manager	Kurt Manufacturing 7	63(612)572-4627
Chris Wiege	Contractor	Climatronics, HAVAC/R 7	63(612)427-4940

Table II-2, Important Contributors to the Project: tact information for contributors and company position is listed be

First, Karl DeWahl who is a senior engineer for the Minnesota Technical Assistance program (MnTAP) served as and an intern advisor. Karl contributed his technical knowledge about the metal finishing industry. Karl also provided valuable advice based on his engineering experience.

Next, Roger Knaus and Dave Muncy who are the current operators of the Metal Finishing Line at the Main St. Plant each supplied information about the history of and current operation of the Metal Finishing Line. Roger also provided warnings about the changes made to the process. Input from Dave included concerns about the current operation procedure.

Jim Sjoselius, Corporate Environmental Health and Safety Manager at Kurt, provided valuable insight into the waste water problems. Jim contributed with his knowledge and experience of health and safety issues regarding the project.

Finally, Chris Wiege who is an independent contractor completed the plumbing necessary for installing the cascades in the Metal Finishing Line. Input from Chris included plumbing options and ideas for constructing the new weir systems.

II. Waste Reduction Options: Machining Division and Kurt Gear Division

- A. Waste Volume
- B. Management Method
- C. Reasons for Researching Option
- D. Cascade Rinse Tanks
- E. Reduce Carry-Over Volume
- F. Characterize Rinse Water
- G. Optimize Fresh Water Flow Rates
- H. Implementation

A. WASTE VOLUME

Currently, five million gallons of waste water is produced annually by the Metal Finishing Line. Before being drained to the sewer all waste water is gathered in a one thousand gallon tank where pH monitoring and adjustment occurs. An additional 10,500 gallons of hazardous material from the same process is disposed of annually. This hazardous material includes 1,500 gallons of chromic acid, four thousand gallons of aluminum deoxidizer, and five thousand gallons of nitric acid. The primary concern is to reduce waste water generation

B. MANAGEMENT METHOD

Presently, the only method of waste management employed is pH adjustment of the waste stream. Figure V-4 in appendix C shows a diagram of the pH adjustment system. This method accounts only for the waste water and not the hazardous materials. Increased documentation of hazardous material disposal and improved maintenance of the waste water will each improve waste management. In addition, improved communication between shift employees will help refine current management methods.

C. REASONS FOR RESEARCHING OPTIONS

The primary reason for researching waste water reduction options is to decrease operating costs for the Metal Finishing Line. In addition, the overall plant waste water discharge will be reduced. This reduction allows the facility to operate within its pre-determined SAC limit which is currently 147 SAC units or 40 thousand gallons daily. Health and safety of process operators is the final reason for system modifications. Analysis of this system will also eliminate inaccurate use of caustic for manual pH adjustment of Tank 11 rinse water and therefore chemical cost will be reduced.

Waste water generation can be reduced directly by cascading rinse tanks and by reducing fresh water flow rates. Although, reducing the . fresh water flow rate cannot be performed unless rinse water quality will not be diminished. Therefore, process changes which reduce contamination of rinse water must occur so that the fresh water flow rates can be optimized. Methods that can be used to reduce this carryover include, drip-time extension, spray-rinse implementation, and basket modification. Finally, development of a cleaning schedule which includes water quality testing will reduce both annual operating costs and process down-time. Specific modifications to the Metal Finishing Line and their benefits will be discussed.

D. CASCADE RINSE TANKS

1. Type of Process Change

Implementation of cascading significantly reduces waste water volume produced by the Metal Finishing Line and decreases the annual operating cost of the process. Counter-current rinsing within the Metal Finishing Line requires equipment modification. This equipment modification includes weir construction and plumbing. In addition, an equipment change will be required to reduce the use of caustic for manual pH adjustment. Specifically, stainless steel tanks will be replaced with poly-propylene tanks. The combination of nitric acid and

ammonium biflouride is corrosive to the stainless steel and after time cause the tanks to crack and leak.

Waste water can be reduced by employing counter-current rinsing or cascading the tanks, as shown in figure II-1. Essentially, fresh water is fed to the final rinse tank. The waste water from that tank is fed to another tank in the line. Theoretically, this scheme can continue until all of the rinse tanks are connected together. The parts are passed in the opposite direction of the water flow. Therefore, the final rinse tank will contain the cleanest water as compared to all of the rinse tanks in the line.



Figure II-1, Simple Schematic of Counter-Current Rinsing: The water from one tank is fed to the one just before it. The final tank in the line receives fresh water.

Counter-current rinsing can be applied to a process where chemical process baths are also utilized. Figure II-2 shows how the concept of cascading rinse tanks can be used in conjunction with chemical tanks. This cascading allows water, that would have been waste, to be re-used. New contaminants are never introduced into the rinse water. Rather chemicals from the process bath are rinsed in one tank and fed to the previous rinse tank in dilute concentrations. In general, the chemicals are passed from one rinse tank to another. Water is fed to the bottom of the tank to force dirt and contaminants away from the tank bottom, over the weirs and out of the tank. Although plumbing codes discourage fresh water from being fed to the bottom of the tank.



Figure II-2, Rinse Tanks Cascaded within a Chemical Process Line: Fresh water is fed to the final rinse tank and its waste water is fed to the rinse tank just before it. The soll contained in the waste water from rinse tank 2 is the same component as in the chemical bath.

Counter-current rinsing has been employed in past and was discontinued because of a lack of sufficient overflow from one tank to the next. Insufficient overflow occurred because the water level in each tank in the cascade series was even. Flow from one tank to the next can be forced by decreasing the water level in each tank. The last rinse tank in the series of cascades will have the highest water level and the first tank in the cascade series will have the lowest water level. For example, in figure II-2 tank 1 will have a lower water level than tank 2.

Four possibilities for cascading rinse tanks within the Metal Finishing Line have been investigated. Figure II-3 shows where cascading can be incorporated into the current system. Calculations in section 1-f of appendix A show how the water level difference was calculated and table III-1 summarizes these water level differences.

 Fluids calculations are shown in section 1-f of appendix A.					
Cascade Connection		Water Level Difference (inches)	•		
Tank 15 to Tank 12	Ť	1.2	1		
Tank 12 to Tank 11		1.0			
Tank 11 to Tank 8	1	1.2			
 Tank 4 to Tank 2		0.64			

Table III-1, Water Level Differences for Cascading Options: Fluids calculations are shown in section 1-f of appendix A.

a. Cascade 1

The first option is to modify the first section of the line. Currently, the second tank remains inactive. This tank can be converted to a rinse tank. Then the third tank, currently the alkaline rinse, can be converted to an etch tank. This conversion, allows the next three tanks to be used as rinse tanks as originally designed. The waste water from tank 4 will also be fed to tank 2 as shown in figure II-3. Essentially, Cascade 1 will connect four rinse tanks—Tank 6, Tank 5, Tank 4, and Tank 2—through counter-current rinsing.

in the set

b. Cascade 2

Cascade 2 will contain three rinse tanks—Tank 12, Tank 11, and Tank 8. A low pH in tank 11 causes the stainless steel tank to corrode and begin leaking water. Therefore, pH is controlled with the manual addition of caustic solution. By feeding the waste water from tank 11 to tank 8, corrosion of tank 8 also becomes a problem. Hence,

polypropylene tanks will replace the two stainless steel tanks. These new tanks will eliminate the need for manual pH monitoring.

c. Include Tank 15 in Cascade 2 Tank 15 can be included in Cascade 2. Because conversion

coating is an option as specified by the customer, not every type of part needs to be dipped into either of the iridite tanks (Tank 13 or Tank 14). Hence, rinse water containing chromic acid may cause a problem when iridite is not specified for the part. Installation of a valve system will prohibit the problem of iridite contamination from occurring. Valves can be used to direct the waste water flow from Tank 15 to either Tank



12 or to drain. Essentially, a valve system will allow cascading only when the iridite tanks (Tank 13 and Tank 14) are in use.

d. Cascade Tank 16 and Tank 15

The other option is to operate Tank 16 and Tank 15 as countercurrent rinsing tanks. Currently, Tank 16 operates as a heated dead rinse and therefore heating costs for Tank 16 will be increased.

2. <u>Benefits</u> of <u>Cascading Rinse</u> <u>Tanks</u>

Appendix A, section 1-b shows the calculations of annual savings and of annual waste water reduction. In each cascade, the fastest previous fresh water flow rate was assumed to be the new fresh water flow rate for the cascade. In addition, it was assumed that the chemical costs for the rinse water would decrease with a decrease in waste water generation. Total cost and savings values are shown for all of the tanks in the Metal Finishing Line and for the rinse tanks alone.

a. Cascade 1

Modification for Cascade 1 will included moving the etch tank (Tank 4) from its current position to Tank 3. Tank 2 is currently not in use and therefore will be converted to a rinse tank. Three dip rinses after the etch tank provide a better rinse than two dip rinse tanks. By including tank 2 in the cascade, waste water generation will be reduced by 264 thousand gallons annually and annual operating costs will decrease by \$1,637.

b. Cascade 2

Implementation of this cascade will reduce waste water generation by 1.9 million gallons each year and an annual savings of \$9,992. Cascade 2 requires the construction of two new tanks. These two tanks will eliminate the safety concerns about handling caustic solution. Chemical costs will also be reduced because caustic solution will only be used in the automatic pH adjustment of the waste water.

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Maintenance of Tank 11 water pH between 9 and 10 requires about a half gallon of 50% caustic solution. When Tank 11 is used, caustic solution is added to the tank manually after each dip-rinse. Acid is rinsed from the parts with this alkaline rinse water. Then the pH of the Rinse water drops drastically. Without any caustic addition, this trend continues until the pH reaches a value of about 2 and maintained for the duration of operation. Figure V-2 in appendix B, section 1-2 shows the pH profile of the rinse water in Tank 11. Hence, maintaining a pH of 9 requires about 10 gallons of 50% caustic solution throughout any one day of operation when Tank 11 is used for rinsing.

c. Include Tank 15 in Cascade 2

By including Tank 15 in Cascade 2, annual waste water generation will be reduced by an additional 282 thousand gallons. A additional operating costs savings of \$1,845 will be experienced. Finally, clean rinse water can be maintained for use after the conversion coating is applied.

d. Cascade Tank 16 and Tank 15

Employing counter-current rinsing with tank 16 and Tank 15 does not result in any monetary or waste water reduction benefits. Although, a clean final rinse can be obtained. Temperature data is found in table V-29 in section 1-b of appendix B.

3. Economic Analysis

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The economics of each cascade option will be discussed and summarized in Table II-2. In each case, the payback period is calculated after taxes assuming a 50% tax rate. In addition, a five year project lifetime and 15% rate of return is assumed. All economic calculations are shown in appendix A, section 1-e in the following tables; Table V-11, Table V-12, Table V-13, Table V-14, and Table V-15.

a. Cascade 1

Cascade 1 only requires plumbing and therefore the capital investment of \$500 is minimal. Down-time can be avoided by modifying the tanks during the cleaning process. Annual savings of \$1,637 or \$819 after taxes will also be small. A payback period of eight months, a discounted cash flow rate of return of 162% and a net present value of \$2,243 can be expected. Based on a five project lifetime the net present value is \$2,243.

b. Cascade 2 tanks |2 - 7|| - 7 8

Implementation of Cascade 2 will lead to a larger annual savings than Cascade 1. After a payback period of 15 months, an annual savings of \$9,992 or \$4,996 after taxes will be experienced. Because of the construction of new tanks, the total capital investment exceeds the minimal costs of plumbing. The tanks, constructed of polypropylene and having a ten year lifetime, will cost \$1,800 each from UNIFAB, Inc. of St. Louis Park. Tank installation will cost an estimated \$200 per tank. Added costs included \$1,000 and \$425 for plumbing and down-time respectively. Ultimately the total capital investment will be \$5,425. The discounted cash flow rate of return is 88% and the net present value is \$11,322.

c. Include Tank 15 in Cascade 2

Including tank 15 in Cascade 2 will save an additional \$1,845 annually or \$923 after taxes. Plumbing costs result in a minimal capital investment of \$500. A seven month payback period and 184% discounted cash flow rate of return can be expected. Finally, a net present value of \$2,592 will be experienced.

d. Cascade Tank 16 and Tank 15

As stated earlier Cascading Tank 16 and Tank 15 will result in no monetary savings. This option will cost \$640 annually due to increased electric cost for heating the fresh water feed to Tank 16. Hence, employing counter-current rinsing to Tank 16 and Tank 15 yields no monetary benefits.

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Table II-2, Economic Analysis Summary for the Cascade Options for the Metal Finishing Line at the Machining and Kurt Gear Divisions: Calculations are based on a five year project lifetime and a 50% tax rate. Appendix A. section 1-e displays all calculations

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Options	Cascade 1	Cascade .2	Include Tank 15 in Cascade 2	Cascade Tank 16 and Tank 15 [°]				
Capital Investment (\$)	500	5,425	500	_				
Annual Savings (\$/year)	1,637	9,992	1,845	-640				
Equipment Lifetime (years)		10						
Payback Period (months)	8	15	7					
Net Present Value (\$/year)	2,243	11,322	2,592					
Discounted Cash Flow Rate of Return	162%	88%	184%					

E. REDUCE CARRY-OVER VOLUME

1. Type of Process Change

Carry-over volume exists in two forms. The first form of carry- over volume is any type of solution that is trapped within holes of parts or freely drains from parts and racks. Extension of drip-time, and modification of the part basket will each reduce this type of carry-over VSMg a sample OF mesh such as used in the basket, RB measure volume. The second type of carry-over volume exists as a film, which adheres to the part and basket. Spray rinsing will reduce the chemical of woder. film that can be carried from one tank to the next. This extrapolator to $^{3}25/b$ or $^{3}25/b$

The use of each process tank dictates the annual carry-over gula for fine lvolume from each tank. For example the alkaline wash tank is needed for every part, but the passivate tank is only used for finishing stainless steel. Spray rinsing installation and basket modification requires equipment changes. Drip-time extension requires a process change.

2. Benefits of Reducing Carry-Over Volume

The reduction of carry-over not only reduces chemical costs, but also allows the reduction of the fresh water flow rate. Therefore chemical, water, and sewer costs can be reduced.

A test was conducted to compare the carry-over from the original drip-time of five seconds to an increased drip time of 30 seconds. Table II-3 shows that the initial carry-over volume is decreased by 60%. This decrease in carry-over volume will decrease the annual chemical costs. For example, if the drip-time were increased and the carry-over volume was reduced by 60%, an annual chemical cost savings of \$3,574 can be expected. Calculations are shown in appendix A, section 1-c.

Table II-3: Carry-Over Volume Estimation for a Typical Load Carry-over was estimated for some drip-time after the basket was moved from one tank to the next. Increasing the drip-time does prevent chemicals from being carried into the next tank and therefore chemical cots will decrease. After the drip-time was increased to 30 seconds, carry-over volume was reduced by as much as 0.38 gallons or 60%

Drip-Time	Volume	Drip-Time	Volume
5 s	0.60 gallons	30 s	0.25 gallons
5 s	0.63 gallons	30 s	0.25 gallons

Because drip-time extension is only an option for the tanks that are not heated, spray-rinsing may be the best option for the heated tanks. Spray-rinsing washes the chemicals back into their respective tanks. This option also provides an additional method for rinsing parts. Spray rinsing will also replenish evaporative losses experienced by the heated process tanks.

A test results showed that the current basket design allows 270 gallons of solution to be carried from one tank to the next each year. By designing the baskets to reduce this carry-over volume up to two thousand dollars in chemical costs can be saved annually. In addition, the process time will not be increased at all.

Current basket design allows for a variety of parts to be metal finished. Baskets can be designed to remove some of the mesh material, but still have the ability to carry the largest parts. The sides of the baskets can be removed or be made smaller. In addition, the bottom of the baskets can be replaced with rails or bars. Small baskets, which fit inside the original basket, can be constructed to hold small parts.

3. Economic Analysis

The first carry-over reduction option, increasing the drip-time, significantly reduces the carry-over volume, but also increases the process time. Although annual chemical costs will decrease by \$3,574, extended process time will potentially cost \$18,889 annually. Process time losses will only be experienced if the line is operating at full capacity. Appendix A, section 1-c shows the savings calculation and the extended process time cost calculation is shown in section 1-c

Process time can also be claimed be decreasing the length of the rinse time. Less contamination will occur because the carry-over volume has been decreased. Hence, less rinsing time is necessary to clean the parts.

Another option of altering the basket design does not increase the process time and will save \$1,423 in annual chemical costs. Calculations are also shown in appendix A, section 1-c. Although, this

value assumes that all basket mesh will be eliminated for every cycle. Capital cost for altering the baskets will only be the cost of labor and has not yet been determined. The final option of spray-rinsing needs further investigation.

F. CHARACTERIZE RINSE WATER TO REDUCE TANK CLEANING

<u>1. Type of Process Change</u>

Currently, a rinse tank is cleaned when rinse water looks 'dirty' or has not been cleaned for 'a while'. Once each week the 'dirty' rinse water is dumped. The tanks are then scrubbed and partially inspected for any visible cracks. Fresh water fills the tank. This cleaning process does not included any prior testing of 'dirty' water. The tanks are drained rather quickly, but scrubbing of one rinse tank requires 45 minutes of downtime. This current system permits wasting rinse water and requires extensive down-time. A maintenance change of characterizing 'dirty' rinse water with conductivity and pH readings can decrease down-time and wasted rinse water. Although, conductivity and pH readings provide indirect measures of contamination. Therefore cleaning limits need to be chosen carefully. Additional care needs to be taken with the conductivity meter. In general conductivity meters are quite sensitive and must be calibrated on a regular basis.

2. Benefits of Characterizing Rinse Water

Some of the rinse tanks need to be cleaned more often than others, but on average each tank is cleaned 36 times per year. Currently, no system exists for determining when rinse water needs to be dumped. If tanks do not need to be cleaned as often operation down-time will be reduced significantly. In addition, waste water generation will be decreased. Conductivity and pH data are located in table V-28 and table V-30 respectively in appendix B section 1-a and section 1-c.

For example, if the tanks are cleaned out only 18 times per year, down-time is reduced by 108 hours annually and waste water generation will be decreased by 72 thousand gallons annually. Annual savings of \$879 can be expected in water and sewer costs and potentially \$9180 in down-time can be saved each year. Down-time savings can only be experienced at full capacity operation. Calculations assume that the tanks are cleaned half as much and hence only 9 thousand gallons of water is used for cleaning. The down-time calculation is shown in appendix A, section 1- b.

3. Economic Analysis

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The only capital cost required to characterize rinse water is \$500 for a bench-top conductivity meter. The actual savings and payback can only be calculated can only be done once it is determined how often the tanks will be cleaned. Although, an economic analysis was conducted on a scenario of cleaning the tanks half as much. By cleaning the tanks half as often \$879 in water and sewer costs can be saved annually after a payback period of 16 months. A 15 % rate of return was assumed. Assuming a 50% tax rate, the annual savings will be \$440. In addition, the net present values after five years will be \$973 and the discounted cash flow rate of return is 84%. Section 1-e in appendix A shows the economic calculations.

In addition to water cost and sewer cost savings, less down-time will be experienced. This decrease in down-time from cleaning ca potentially result in an additional annual savings of \$9,180 for a total annual savings of \$10,059. The new payback period is then only one month with a discounted cash flow rate of return of 1008%. The net present value is \$16,360 for a five year project lifetime.
G. OPTIMIZE FRESH WATER FLOW RATES

1. <u>Type of Process Change</u>

The present process does not control any of fresh water flow rates. Although, three rinse tanks—Tank 12, Tank 8, and Tank 6—each have a solenoid valve that times the flow of fresh water. The solenoid valves have programmed intervals to deliver fresh water for seconds and wait for 10 seconds. The remaining tanks each have a manual valve which delivers fresh water. Optimization of fresh water flow rates will keep clean rinse water from being wasted. In addition, the solenoid valves can be adjusted to deliver fresh water only when the rinse tanks are being used. Each of these options will require a process change.

2. <u>Benefits of Optimizing Water Flow Rates</u>

The conductivity and pH of the rinse water was monitored periodically for a number of weeks. During this time an experiment with decreased flow was conducted. The test results showed that by decreasing the fresh water flow rate, the water quality did not decrease significantly. This test suggested that the current fresh water flow rates allow virgin rinse water to be wasted. Essentially, optimization of fresh water flow rates will efficiently utilize rinse water and will ultimately reduce operating costs.

3. Economic Analysis

Fresh water flow rates can only be optimized after cascading is implemented. Ideally, the flow rates should be verified after any type of process change. Optimization of flow rates will cost nothing, but will save on annual water and sewer costs.

H. IMPLEMENTATION

Each of the options has the possibility to reduce waste water generation and to decrease annual operating costs. The changes require either small equipment changes or simple process modifications. The options of employing counter-current rinsing was fully investigated. Preliminary research and testing was done on the remaining options, and further investigation may be necessary before any modifications can be made. Progress of each waste reduction option is found in the Table II-4. In addition, cost savings and waste reduction volume is included.

Table II-4, Waste Reduction Option Implementation Summary: Cost savings include water costs, sewer costs, RO system costs, and chemical costs.

Waste Reduction Option	Waste reduced (gal/yr)		Cost Savings (\$/yr)	Status				
Cascade Rinse tanks	1							
Cascade 1	2	64,000	1,637	implemented				
Cascade 2	1,	926,000	9,992	not yet				
Include Tank 15 in Cascade 2	2	82,000	1,845	implemented recommended				
Cascade Tank 16 and Tank 15		0	-640	not feasible				
Reduce Carry-Over Volume*	Waste	Chemicals (/yr)						
Extend Drip-Time	1950 6,814 lb		2,513	recommended				
Design New Basket	1350	3,364 lb 47 gal	1,423	recommended				
Spray-Rinsing				recommended				
Characterize Rinse Water*	72,000		72,000		72,000		10,059	recommenced
Optimize Flow Rates*	922,000		5,716	recommended				

*estimated values based on examples

1. Cascade Rinse Tanks

a. Cascade 1

Cascade 1 was recently implemented and therefore problems cannot be reported at this time. One anticipated problem is the inability to have enough overflow. The fresh water flow rate will need to be adjusted accordingly. Although, at the time of implementation no initial problems were sighted. Figure V-5 in appendix C shows a detailed diagram of the weir construction of Tank 2.

b. Cascade 2

Problems with implementation occurred with obtaining materials for modifications. In addition, problems with stopping production became an issue. Materials are currently ordered and this option will be implemented when the new tanks arrive.

c. Include Tank 15 in Cascade 2

Quality issues prohibit this option from being implemented immediately. Although, with testing and success of the other cascades the Metal Finishing Line can easily be modified to included this option.

d. Cascade Tank 16 and Tank 15

This is option is clearly not feasible because of the added cost for heating. Although if rinse water quality becomes an issue, the Metal Finishing Line can be adapted to accommodate this cascade.

2. <u>Reduce</u> Carry-Over Volume

Extension of the drip-time requires additional testing. Another drip-time (possibly 15 seconds) should be tested. This test will show if the carry-over volume plateaus at a given drip-time. The difficulty of modifying the baskets needs to be investigated. Spray-rinsing will definitely help reduce the carry-over volume and replenish evaporative losses. Although, the economic feasibility needs to be investigated. Concern about increasing the entire process time has been expressed. Once the drip-time is increased, process time can be saved by reducing the allotted time for rinsing. Because chemicals will be allowed a longer time to drain less rinsing is necessary. This option requires contact with customers because of a procedural change. In general, contact of customers is resisted due to the number of customers and variety of products.

3. Characterize Rinse Water to Reduce Tank Cleaning

Better characteristics need to be determined before this option can be implemented. The current method of defining 'dirty' rinse water is so subjective that it is difficult to set conductivity and pH limits. In addition, tanks are not cleaned when the rinse water 'looks dirty' if production cannot be halted. Essentially, rinse tanks are only cleaned if it is convenient to stop production.

4. Optimize Fresh Water Flow Rates

This option cannot be implemented until each of the cascades are in place. Ideally, the fresh water flow rates should be adjusted each time a change is made to the metal finishing line.

III. Waste Reduction Options: Automatic Division

- A. Waste Volume
- B. Management Method
- C. Reasons for Researching Option
- D. Cascade Rinse Tanks
- E. Spray-Rinsing
- F. RO Reject Options
- G. Implementation

A. WASTE VOLUME

The Automatic Division, currently discharges five million gallons of waste water annually. The majority of this water is used for washing spacers. Specifically, the Carousel Washer System generates just over three million gallons of waste water each year and the Crest Washer Systems produce just over one million gallons of waste water annually." The remaining waste water is generated by the RO System, domestic use and other machines.

B. MANAGEMENT METHOD

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No current method exists for managing waste water. Although, part quality is thoroughly tested each day. Karl DeWahl from MnTap was contacted in March 1997 about the waste water generation. Appendix D is a copy of his report of the situation. In addition, table V-33 in section 2-a of appendix B lists the original conductivity data from his visit.

C. REASONS FOR RESEARCHING OPTION

The primary reason for investigating waste reduction options is to avoid a SAC liability. The facility has a SAC baseline of 43 units or 12 thousand gallons per day, but operates at 81 units or 22 thousand gallons per day. Each SAC unit greater than the baseline limit costs \$950. Hence, the facility will be charged \$36,100 for 38 units greater than the allowed baseline.

Three general process modifications and equipment changes can individually reduce waste water generation. Rinse tanks within the carousel washer and crest washers can be cascaded. Additional spray rinsing can be implemented in the carousel washer to reduce waste water generation significantly. Finally, two options exist for the RO reject water. The first option is to obtain a permit for RO reject discharge and the other is to use the RO reject water for the carousel washer.

D. CASCADE RINSE TANKS

1. Type of Process Change

Currently, two sets of tanks—Tank 4 and Tank 5, and Tank 6 and Tank 7—employ counter-current rinsing within the Carousel Washer System. These two sets can be connected together for only one series of cascaded tanks. One of the Crest Washer Systems can also be modified to included a cascade. Specifically, waste water from Tank N5 can be used to feed Tank N4. Plumbing modifications will be necessary for cascading rinse tanks.

2. Benefits of cascading Rinse Tanks

By cascading the tanks in the Carousel Washer System, waste water generation can be reduced by 297 thousand annually or by three SAC units daily. Annual savings will be \$892 and the SAC liability will be reduced by \$2,850. An additional waste water reduction of 700 thousand gallons annually or seven SAC units daily. Annual savings will increase by \$1,318 and SAC liability will decrease by \$6,650

3. Economic Analysis

Calculations, in appendix A (section 2-b and section 1-d), were made after taxes and assuming a 50% tax rate. In addition, a five year project lifetime and 15% rate of return was assumed. It was also assumed that SAC liability reduction was only experienced within the first year of the project. Results are tabulated in Table III-1.

Plumbing modifications for cascading in the Carousel Washer System will cost \$1000. After a nine month payback period, a gross annual savings of \$892 or after taxes a savings \$446 will be experienced. An additional savings for SAC liability of \$2,850 is also possible. The net present value will be \$1,735 and the discounted cash flow rate of return will be 122%.

A capital investment of \$1,000 includes all plumbing modifications needed to cascade Tank N5 and N4. After three months, a gross annual savings of \$1,318 or after taxes a savings of \$659 will be experienced. In addition, SAC liability will be decreased by \$6,650. The discounted cash flow rate of return will be 319% and the net present value will be \$4,100.

Table III-1, Economic Analysis Summary for the Cascade	
Options for the Automatic Division:	
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Options	Cascade in Carousel Washer	Cascade in Crest Washers
Capital Investment (\$)	1,000	1,000
Annual Savings (\$/year)	892	9,318
SAC Liability Reduction (\$)	2,850	6,650
Payback Period (months)	9	3
Net Present Value (\$/year)	1,735	4,100
Discounted Cash Flow	346%	319%
Rate of Return		

Calculations are based on a five year project lifetime, 15% rate of return, and a 50% tax rate. Appendix A, section 2-d displays all calculations.

E. SPRAY-RINSING

1. Type of Process Change

Spray-rinsing is currently used within the Carousel Washer System and the Crest Washer Systems. After equipment modifications, an additional spray-rinse can be employed within the Carousel Washer System. Tank 2, a dip rinse tank in the Carousel Washer System, can be replaced with a spray-rinsing system and waste water from Tank 4 can be used for spray-rinse water. The current spray-rinses within the Crest Washer Systems can be modified to use waste water from the dip-rinses rather than fresh water. Specifically, Tank O3 waste water can be used to feed the spray-rinse in Tank O2 and Tank N4 waste water can be used to feed the spray rinse in Tank N3.

2. Benefits of Spray Rinsing

By installing additional spray-rinsing in the Carousel Washer System, annual waste water generation can be decreased by one million gallons annually or by 10 SAC units daily. Hence annual costs are decreased by \$3,015 and the SAC liability is decreased by \$9,500. Annual waste water generation can be decreased by an additional 877 thousand gallons or nine SAC units daily if modifications are made to the Crest Washer Systems. Annual savings will increase by \$2,753 and SAC liability will decrease by \$8,550.

3. Economic Analysis

Appendix A (section 2-b and section 1-d), shows the economic analysis calculations. These calculations assume a 50% tax rate, a five year project lifetime and 15% rate of return. It was also assumed that SAC liability reduction was only experienced within the first year. Payback period calculations were made using an after taxes cash flow. Table III-2 summarizes the results.

Installation of spray-rinsing in the Carousel Washer System will save the most annually and will reduce the SAC liability the most as compared to all options. After a capital investment of \$1,500 and a payback period of two months, an annual savings of \$3,015 or after taxes a savings of \$1,508 can be expected. The SAC liability can also be reduced by \$9,500. The net present value is \$7,684 and the discounted cash flow rate of return is 346%

Modification of the Crest Washer Systems will require a capital investment of \$1,000. After a one month payback period, an annual savings of \$2,753 can be expected. After taxes the annual savings will be \$1,377. The SAC liability can also be reduced by \$8,550. The net present value is \$7,332 and the discounted cash flow rate of return is 493%.

Options	Spray-Rinse in Carousel	Spray-Rinse Modifications in Crest Washers		
Capital Investment (\$)	1,500	1,000		
Annual Savings (\$/year)	3,015	2,753		
SAC Liability Reduction (\$)	9,500	8,550		
Payback Period (months)	3	1		
Net Present Value (\$/year)	7,684	7,332		
Discounted Cash Flow	346%	493%		
Rate of Return				

Table III-2, Economic Analysis Summary for the Spray-Rinsing Options for the Automatic Division:

Calculations are base	d on a five year project lifetime, 15% rate of return,
and a 50% tax rate.	Appendix A, section 2-d displays all calculations.

F. RO REJECT OPTIONS

1. Type of Process Change

Essentially, two options exist for the RO reject water. The water can be discharged to the storm sewer with a NPDES permit. The other option is to use the RO reject water in the Carousel Washer System, which is an actual procedural change. The current procedure uses city well water in most rinse tanks.

2. Benefits of RO Reject Options

By discharging the RO reject water through the storm sewer or by using this water to feed the Carousel Washer System, waste water will be reduced by 937 thousand gallons per year or by nine SAC units per day. Obtaining a permit will only allow the SAC liability to be decreased, but the option of using the RO reject water for the Carousel Washer System will add water and sewer savings. Specifically, annual savings will be \$3,281 and the SAC liability will be decreased by \$8,550. The increased regulatory burden of maintaining the permit will also be avoided by using RO reject for the carousel washer.

<u>3. Economic Analysis</u>

Appendix A (section 2-b and section 1-d) shows the economic analysis calculations. These calculations assume a 50% tax rate, a five year project lifetime and 15% rate of return. Payback period was calculated with an after taxes cash flow. It was assumed that SAC liability decreases will only be experienced in the first year. Table III-3 summarizes the results

By using RO reject water to feed the Carousel Washer System, \$3,281 can be saved annually or after taxes an annual savings of \$1,641 will be experienced. Capital investment will be \$1,500, which includes a

storage tank for \$500 and any plumbing. A payback period of three months is expected with a net present value of \$1,640. The discounted cash flow rate of return is 328%. The option of obtaining a NPDES permit requires an annual fee of \$1200 and an application fee of \$85.

Table III-3, Economic Analysis Summary for the RO Reject Options for the Automatic Division:

Calculations are based on a five year project lifetime, 15% rate of return, and a 50% tax rate. Appendix A, section 2-d displays all calculations.

Options	NPDES Permit	RO Reject for Carousel
Capital Investment (\$)	85	1,500
Annual Savings (\$/year)	-1,200	3,281
SAC Liability Reduction (\$)	8,550	8,550
Payback Period (months)	·	3
Net Present Value (\$/year)	·	1.640
Discounted Cash Flow		328%
Rate of Return		

G. IMPLEMENTATION

All of the options, except for one, are recommenced. Each option will reduce waste water generation and hence, decrease annual water and sewer costs. In addition, the options can significantly reduce SAC liability. Table II-4 summarizes the savings possibilities, waste reduction potential, and status of each option.

Wasta	Wasta Wasta SAC Cost SAC Status								
Reduction Option	Waste Reduced (gal/yr)	Reduced (units)	Savings (\$/yr)	SAC Liability Savings (\$)	Status				
Cascade in Carousel	297,480	3	892	2,850	recommended				
Cascade in Crest Washer	700,150	7	1,318	6.650	recommended				
Spray Rinse in Carousel	1,005,000	10	3,015	9,500	recommended				
Spray Rinse Modifications in Crest Washers	876,850	9	2,753	8,550	recommended				
NPDES Permit	0	9	-1200	8,550	not recommended				
RO Reject for Carousel	937,300	9	3,281	8,550	recommended				

Table III-4, Implementation Summary for Waste Reduction Options: Cost savings include water costs, sewer costs, and RO system costs. In addition SAC liability savings is listed. Each SAC unit denotes 274 gallons per day.

Essentially, implementation of each of the options is resisted for two reasons. First, any type of change to the current cleaning system risks harming product quality. The second problem is a general resistance to change and a low priority status of water conservation.

The option of obtaining a permit is not recommenced because of increased regulatory burden of reporting and because of the increased cost of maintaining the permit. In addition, a permit does not decrease the generation of waste water.

IV. Waste Reduction Options: Industrial Product Division

The Industrial Products Division performs metal cleaning and finishing for bomb casings. The parts are cleaned in one line of tanks and finished in another line of tanks. The area of concern is the second line of tanks where the casings are finished. In this line, the parts are dipped into an iridite tank and proceed through a series of three diprinse tanks. The carry-over volume from the iridite tank is so large that the first rinse tank quickly becomes contaminated and needs to be disposed of as hazardous material.

A preliminary analysis of the situation was done when the line was not in operation. Therefore only qualitative suggestions to reduce hazardous material disposal can be made. Carry-over volume can be reduced directly by increasing the drip-time over the process tank, or by tilting the casing for better drainage. Spray-rinsing can be used either above the process tank or in place of the first drip rinse. Finally, the first dip-rinse tank can be changed to a drip tank. A drip tank serves as an empty tank where solution can drain from the part and later be pumped back into the original process tank. Each of these options can be investigated for possible application and economic feasibility.

V. Appendices

A. Calculations

B. Test Results

C. Process Drawings

D. Additional Information

E. List of Resource People

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F. Bibliography

A. CALCULATIONS

1. Machining Division and Kurt Gear Division

An example calculation is shown for each set of calculations. If more than one situation occurred, the spreadsheets for each different situation follow the example calculation.

a. Original Operating Costs and Water Usage

The evaporation rates were determined using figure V-1. Each heated tank has a temperature range, therefore the evaporative rate was calculated for each limit. Then an average value was found and used in further calculations. Tank dimensions are 78 inches by 43 inches. A sample calculation for Tank 1 is shown and table V-1 summarizes the evaporation rates for the four heated tanks.



Figure V-1, Evaporation Rate Trend: Evaporation rate is found assuming relatively still air (D1). The dimensions of the tank are 78 inches by 43 inches.

Sample Calculations for Tank 1

Surface Area

$$(78 \text{ in})(43 \text{ in})\left(\frac{144^{2}}{12^{2} \text{ in}^{2}}\right) = 23.29\text{ ft}^{2}$$

Tank 1 150°F+0 180°F
• 150°F 0.1qal/ft²/m (fromplot)
 $(0.1 \text{ gal} \text{ lm})(23.29 \text{ ft}^{2}) = 2.33 \text{ gal/m}$
 180°F 0.2qal/ft²/m (from plot)
 $(0.2qal/ft^{2}/m)(23.29 \text{ ft}^{2}) = 4.66 \text{ gal/m}$
Average $(2.33 \pm 4.66)^{1/2} \text{ gal/m}$
 $= 3.5 \text{ gal/m}$

Table V-1, Evaporation Rates for the Heated Tanks: Evaporation is negligible when the water temperature is less than 90°F

Tank	Temperature Range (°F)	Evaporation Rate (gal/hr)
1	150-180	3.5
4	100-160	2.0
13	120-125	1.1
14	130-140	1.5

Chemical costs were based on the amount purchased in one year. Table V-2 shows the chemical prices, chemical volume, and annual costs. The chemical usage column shows the total amount of chemical used in one year. The chemical process tanks are changed periodically throughout the

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Appendix A

year. Pure chemical is not added to the tank. Instead a solution of chemical dissolved in water is used to fill the tank. Table V-2 also shows the concentration of each process bath. The chemical changes column shows the amount of chemical used when the tanks are cleaned. Finally, the extra column shows the amount of extra chemical used for replenishing the process bath. It was assumed that this volume was lost from carry-over.

Table V-2: Annual Chemical Costs:

	All v	alues	are o	n an	annual	basis.	Prices	were	found	on	billina	statements
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		Chemical			1 A A		Carry-Over			
	Tank	Usage		Changes		Extra		(gal)	Price	per
Alkaline	1	2,700	lb	2,250	lb	450	lb	900	\$0.95	lb
Etch	4	2,571	lb	2,256	lb	315	lb	840	\$0.82	lb
Deoxidizer	7	367	gal	300	gal	67	gal	1,340	\$7.60	gal
Passivate	9	4,497	lb	2,943	lb	1,554	lb	264	\$0.18	lb
Nitric	10	85,356	lb	52,965	1b	32,391	lb	2,752	\$0.18	lb
Pik-Aid	10	2,876	lb	1,500	lb	1,376	lb	2,752	\$2.56	lb
Clear	13	70	lb	32	lb	38	lb	608	\$6.60	1b
Yellow	14	350	lb	63	lb	288	lb	2,300	\$9.00	lb

	Annual Costs			Proce Conc	ess Tank entrations
Tank	Changes	Extra	Total Cost	Tank	
1	\$2,137.50	\$427.50	\$2,565.00	1	8 oz/gal
4	\$1,849.92	\$258.30	\$2,108.22	4	6 oz/gal
7	\$2,280.00	\$509.20	\$2,789.20	7	5%
9	\$517.97	\$273.44	\$791.41	9	50%
10	\$9,321.84	\$5,700.82	\$15,022.66	10	100%
10	\$3,840.00	\$3,522.56	\$7,362.56	10	8 oz/gal
13	\$211.20	\$250.80	\$462.00	13	1 oz/gal
14	\$562.50	\$2,587.50	\$3,150.00	14	2 oz/gal
Totals	\$20,720.93	\$13,530,12	\$34.251.05		

Fresh water flow-rates were determined using the bucket method. The amount of time needed to fill a five gallon pail was recorded. Three measurements were taken and the average flow-rate was calculated from these measurements.

The rinse water is changed an average of 36 times per year. Each time 500 gallons of water is drained through the sewer. Hence, an

Appendix A

additional 18 thousand gallons was added to the total water usage and generation.

Water and sewer charges are found directly on billing statements. The disposal charge for hazardous materials is specific for each material and were found on account statements. The value for the RO system is based on the materials needed for a given time period and the amount of RO water produced during this time period. Material cost was found on a purchase order.

It was estimated that fresh water is fed to the tanks for four thousand hours per year. Three tanks—Tank3, Tank 11, and Tank15—have manual valves and hence the water is fed to these tanks for the full time. The remaining tanks—Tank 6, Tank 8 and Tank 12—have automated valves which alternate between feeding water and not feeding water. Therefore fresh water is fed to these tanks only half the time and two thousand hours per year was used for calculation purposes.

Table V-3 shows the current operating costs for the Metal Finishing Line. Additional chemical costs are for waste pre-treatment. The alkaline solution cannot be frothy when emptied into the sewer and the etch solution must be neutralized with sulfuric acid before sewer disposal. The caustic and acid costs are for the automatic pH adjustment system. It was assumed that each rinse tank utilizes equal amounts of chemical for pH adjustment. Although, Tank 11 consume more caustic solution because of manual pH adjustment.

	(gai/hr)		Water (gal	/yr)			Price Data	(\$/aai)			ר ד
ank	Evaporation	Flow	Generatio	n Evaporation	Usage	Disposal	Disposal	Water	Sewer	DO Sustam	1
1	3.5		3,500	29,400	32,900	Sewer	0.00	0.001	0.0025	0.0007	4
2							0.00	0.001	0.0025	0.0027	4.
3		70.5	300,000		300.000	Sound	000	0.001	0.0025	0.0027	(Verni
4	2		12,000	16.800	28,800	Sewer	0.00	0.001	0.0020	0.0027	TUCC
5		450	918,000	a sana ana ana ana ana ana ana ana ana a	18 000	Semior	0.00	0.001	0.0025	0.002/	RANDA
6		0	18.000		918 000	COMO	0.00	0.001	6.0023		ico oo
7			4,000	1	4.000	RCRA	1 51	0.001	0.0000	0.0007	10000
8		540	1,098,000	Constant generation	1.098.000	Smapr	0.00	0.001	0.0000	0.0027	1-1400
9	1.1		500	9,240	9.740	RCRA	2 49	0.001	0.0000	0.0007	RUW
10			4,500		0	RCRA	3.27	0.001	0.0000	0.0027	
11	Section of the	211.5	864,000	a second	864.000	COMOL	0.00	0.001	0.0000	0.0027	15/12/10
12		600	1,218,000		1 218 000	Setuer	0.00	0.004	CLOUDED	0.0000	18000
13			500		500	RCRA	2 01	0.001	0.0000	0.0007	17000
14			1,000	1	1,000	RCRA	2.01	0.001	0.0000	0.0027	
15		70.5	300.000	Manager and the	300 000	Sowar	2.01	0.001	0.0000	0.002/	151000
16	1.5	0	18,000	12.600	30.600	sower	- A 00	0.001	0.0020	0.0027	lation
		Total	4.760.000	68.040	4 823 540			0.001	5, 5, 52 AD	DADDZ/	13000
		Water	4,749,500	68.040	4 808 300						T
		Hazardous	10,500	~)	a walnum	0 - 2734	200 PAU			1	49,000 q
			,	rms	e vou an	John - a	L'ELAND	in A.u		_	
1	Annual Costs	(\$/vr)			Chemical	V U U V M C = q	140,000				tames
ank	Disposal	Water	Sewer	RO System	Glenneard	USE (aryr)	A11				1
				ite eystem	01 0014		All	1001			
1	0.00	22.00	0.75	00.00	Clep 83M	Defoam					
2	0.00	32.90	0.75	88.83	2,565.00	390.00	2,955.00	\$3,085.48			
	0.00	0.00	0.00	0.00			0.00	\$0.00			
a	0.00	200.00	750.08	D. to on	Caustic	Acid			1	, l, .	
	0.00	300.00	156.00	810.00	190.00	3.23	193.23	\$2,053.23	1 voto	met \$1	Lean 1
4	0.00	28.00	20.00		Clepo 30B	Acid			nau		1000
	0.00	20.00	30.00	//./6	2,108.22	1,415.50	3,523.72	\$3,660.28	6 . 10 0		
A	0.00	40.00	0.005.00		<u>Caustic</u>	Acid			Server	425	'nγ
a	0.00	10.00	2,295.00	48.60	190.00	3.23	193.23	\$2,554.83		40.00	S Bar
<u></u>	0.00	AFOTE	45.00	2,478.60	95.00	1.62	96.62	\$3,538.22			r 16W
7+	6.040.00				Clepo 503	L				hyperson and the state of the s	2011-10-10-10-1-1-1-1
<u>'</u>	0,040.00	4.00	0.00	10.80	2,789.20		2,789.20	\$8,844.00		12.20	1.
0	All the	4.000.00			Caustic	Acid				1-6-6	100
ONCON	0.00	1,098.00	2,745.00	2,964.60	190.00	3.23	193.23	\$7,000.83		*	· - *
_ 					Acid	Pik Aid					
¥	1,245.00	9.74	0.00	26.30	791.41	0.00	791.41	\$2,072.45			
U	14,715.00	0.00	0.00	0.00	15,022.66	7,362.56	22,385.22	\$37,100.22			
Same and					Caustic	Acid					
	0.00	864.00	2,160.00	0.00	380.00	3.23	383.23	\$3,407.23			
2	0.00	1,218.00	3,045.00	3,288.60	190.00	3.23	193.23	\$7.744 83			
					Iridite	Nitric					
3	1,005.00	0.50	0.00	1.35	462.00	200.00	662.00	\$1,668.85			
4	2,010.00	1.00	0.00	2.70	3,150.00	200.00	3,350.00	\$5,363.70			
							-,	+0,000.70			
	[1		Caustic	Acid	1	1			
5	0.00	300.00	750.00	810.00	190.00	Acid 3.23	193 23	\$2 053 23			

	Disposal	Water Sewer RO System	Chemicals	Total
Ali	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402,22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
	0.0%	98.4% 99.7% 98.1%	4.1%	31.6%

b. Annual Savings and Water Reduction

A sample calculation is shown for Cascade 2. Table V-4 shows the results for Cascade 1, Table V-5 shows the results for Cascade 2, Table V-6 shows the results for including tank 15 in cascade 2, and Table V-7 shows the results for cascading Tank 16 and Tank 15. Annual savings for cleaning the tanks less often are shown in table V-8. It was assumed that the rinse tanks would be cleaned half the time. Potential savings from decreased down-time is not included in this table, but the calculation is also shown.

Sample Calculations for Annual Savings and Decreased Down-Time

Tank 8 cost for Cascade 2. New Operating Cost. Chemical cost 190.00 + 3.23. = \$193.23/year assume 600 gol/h for the new flow rate. (600 gal) (2000 hr) = 1,200,000 gal/year generation A from automated value system from parta. from cleaning. 18,000 gallyear. total generation. = 1,218,000 gal/year total usage = 18,000 gal/year. Remaining water is fed to tank 12. in the Cascado

Sample Calculations continued Nater cost. $\left(\frac{18,000\,\text{cost}}{100\,\text{cost}}\right) \left(\frac{15,000}{100\,\text{cost}}\right) = \frac{16}{100\,\text{cost}} = \frac{16}{100\,\text{cost}} \frac{1000\,\text{cost}}{100\,\text{cost}}$ Seven (201: [1,218,000.00] = = = = =,045/year RO COST (18,000-40)/40) (#0,0027) = #48.60/4001 Total cost for Tanks = \$3,304,83 as shown in Table V-5 Decreased Down-Time Potential Southas 45 minutes to dean I tank then for stanks and clean helt as much. clean 18 times per year (or iss times pur war) (18 cloon) (<u>stanks</u>) = 144 tapiks (<u>5175 m</u>) = 103 hr year (<u>clean</u>) = 144 tapiks (<u>5175 m</u>) = 103 hr year (<u>stanks</u>) = 103 hr 108 hrs saved per year @ \$5 per mour (108kh) (#85) = [#9,180/4pan Fotential Shvings

	(gal/hr)		Water (gal/y	r)			Price Data (\$	(gal)		
Tank	Evaporation	Flow	Generation	Evaporation	Usage	Disposal	Disposal	Water	Sewer	RO System
1	3.5		3,500	29,400	32,900	sewer	0.00	0.001	0.0025	0.0027
2	•	450	918,000		18,000	sewer	0.00	0.001	0.0025	0.0027
3	2		12,000	16,800	28,800	sewer	0.00	0.001	0.0025	0.0027
4	a desta de la	0	18,000		18,000	sewer	0.00	0.001	0.0025	0.0027
5		0	18,000		18,000	sewer	0.00	0.001	0.0025	0.0027
<u> </u>		0	18,000		918,000	sewer	0.00	0.001	0.0025	0.0027
7			4,000		4,000	RCRA	1.51	0.001	0.0000	0.0027
		540	1,098,000		1,098,000	sewer	0.00	0.001	0.0025	0.0027
9	1.1		500	9,240	9,740	RCRA	2.49	0.001	0.0000	0.0027
10			4,500		0	RCRA	3.27	0.001	0.0000	0.0027
	a share and a second	211.5	864,000		864,000	sewer	0.00	0.001	0.0025	0.0000
12		600	1,218,000		1,218,000	sewer	0.00	0.001	0.0025	0.0027
13			500		500	RCRA	2.01	0.001	0.0000	0.0027
14			1,000		1,000	RCRA	2.01	0.001	0.0000	0.0027
15	and a standard state	70.5	300,000		300,000	sewer	0.00	0.001	0.0025	0.0027
16	1.5	0	18,000	12,600	30,600	sewer	0.00	0.001	0.0025	0.0027
	Total	New	4,496,000	68,040	4,559,540					
	gai/yr	Original	4,760,000	68,040	4,823,540					
		Reduced	264,000	0	264,000					

New	4,496,000	68,040	4,559,540
Original	4,760,000	68,040	4,823,540
Reduced	264,000	0	264,000
	5.5%	0.0%	5.5%
New	4,485,500	68,040	4,544,300
Original	4,749,500	68,040	4,808,300
Reduced	264,000	0	264,000
	5.6%	0.0%	5.5%
New	10,500		
Original	10,500		
Reduced	0		
	0.0%		
	New Original Reduced New Original Reduced New Original Reduced	New 4,495,000 Original 4,760,000 Reduced 264,000 5.5% 5.5% New 4,485,500 Original 4,749,500 Reduced 264,000 5.6% 5.6% New 10,500 Original 10,500 Reduced 0 0.0% 0.0%	New 4,495,000 68,040 Original 4,760,000 68,040 Reduced 264,000 0 5.5% 0.0% New 4,485,500 68,040 Original 4,749,500 68,040 Original 4,749,500 68,040 Reduced 264,000 0 5.6% 0.0% New 10,500 Original 10,500 Reduced 0 0.0% 0

	Annual Costs	;(\$/yr)			Chemical C			
Tank	Disposal	Water	Sewer	RO System			All	Total
					Clep 83M	Defoam		
1	0.00	32.90	8.75	88.83	2,565.00	390.00	2,955.00	\$3,085.48
					Caustic	Acid		
2	0.00	18.00	2,295.00	48.60	190.00	3.23	193.23	\$2,554.83
					Clepo 30B	Acid		
3	0.00	28.80	30.00	77.76	2,108.22	1,415.50	3,523.72	\$3,660.28
			4		Caustic	Acid		
4	0.00	18.00	45.00	48 60	95.00	1.62	96.62	\$208.22
5	0.00	18.00	45.00	48.60	95.00	1.62	96.62	\$208.22
6	0.00	918.00	45.00	2,478.60	95.00	1.62	96.62	\$3,538.22
			3		Clepo 503			
7	6,040.00	4.00	0.00	10.80	2,789.20		2,789.20	\$8,844.00
					Caustic	Acid		
8	0.00	1,098.00	2,745.00	2,964.60	190,00	3.23	193.23	\$7,000.83
					Acid	Pik Aid		
9	1,245.00	9.74	0.00	26.30	791.41	0.00	791.41	\$2,072.45
10	14,715.00	0.00	0.00	0.00	15,022.66	7,362.56	22,385.22	\$37,100.22
					Caustic	Acid		
11	0.00	864.00	2,160.00	0.00	380.00	3.23	383.23	\$3,407.23
12	0.00	1,218.00	3,045.00	3,288.60	190.00	3.23	193.23	\$7,744.83
					Iridite	Nitric		
13	1,005.00	0.50	0.00	1.35	462.00	200.00	662.00	\$1,668.85
14	2,010.00	1.00	0.00	2.70	3,150.00	200.00	3,350.00	\$5,363.70
					Caustic	Acid		
15	0.00	300.00	750.00	810.00	190.00	3.23	193.23	\$2,053.23
16	0.00	30.60	45 00	82.62	95.00	1.62	96.62	\$254.84

New Costs

Totals	Disposal	Water Sewer RO System	Chemicals	Total
All	\$25,015.00	\$4,559.54 \$11,213.75 \$9,977.96	\$37,999.18	\$88,765.43
Rinse	\$0.00	\$4,482.60 \$11,175.00 \$9,770.22	\$1,542.63	\$26,970.45
%Rinse	0.0%	98.3% 99.7% 97.9%	4.1%	30.4%

Old Costs

14 44969				
Totals	Disposal	Water Sewer RO System	Chemicals	Total
All	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
%Rinse	0.0%	98.4% 99.7% 98.1%	4.1%	31.6%

Savings

Totals	Disposal	Water	Sewer	RO System	Chemicals	Total
All	\$0.00	\$264.00	\$660.00	\$712.80	-\$0.01	\$1,636.79
Rinse	\$0.00	\$264.00	\$660.00	\$712.80	-\$0.01	\$1,636.79
					· · · · · · · · · · · · · · · · · · ·	

- NO	wrAnt	
Jus .	4255	hr/yr

Table V-5, Cascade 2: a water reduction for the rinse tanks alone and for all of the tanks. N waste Annual savinos and

	(gal/hr)		Water (gal/y	r) /			Price Data (\$/gal)					
Tank	Evaporation	Flow	Generation	Evaporation	Usage	Disposal	Disposal	Water	Sewer	RO System			
1	3.5		3,500	/ 29,400	32,900	sewer	0.00	0.001	0.0025	0.0027			
2							0.00	0.001	0.0025	0.0027			
3		70.5	300,000		300,000	sewer	0.00	0.001	0.0025	0.0027			
4	2		12,000	16,800	28,800	sewer	0.00	0.001	0.0025	0.0027			
5		450	918,0002		18,000	sewer	0.00	0.001	0.0025	0.0027			
6		0	18,000		918,000	sewer	0.00	0.001	0:0025	0.0027			
7			4,000		4,000	RCRA	1.51	0.001	0,0000	0.0027			
8		600	1,218,000		18,000	sewer	0.00	0.001	0.0025	0.0027			
9	1.1		500	9,240	9,740	RCRA	2.49	0.001	0.0000	0.0027			
10			4,500		0	RCRA	3.27	0.001	0.0000	0.0027			
- 11		0	18,000		18,000	sewer	0.00	0.001	0.0025	0.0027			
12		0	18,000	e e participation de la	1,218,000	sewer	0.00	0.001	0.0025	0.0027			
13			500		500	RCRA	2.01	0.001	0,0000	0.0027			
14			1,000		1,000	RCRA	2.01	0.001	0.0000	0.0027			
15		70.5	300,000		300,000	Sewer	0.00	0.001	0.0025	0.0027			
16	1.5	0	18,000	12,600	30,600	sewer	0.00	0.001	0.0025	0.0027			

1.9	U	10,000	12,000	1 00,000
Total	New	2,834,000	68,040	2,897,540
gal/yr	Original	4,760,000	68,040	4,823,540
	Reduced	1,926,000	0	1,926,000
		40.5%	0.0%	39.9%
Water	New	2,823,500	68,040	2,882,300
	Original	4,749,500	68,040	4,808,300
	Reduced	1,926,000	0	1,926,000
		40.6%	0.0%	40.1%
Hazardous	New	10,500		
	Original	10 500		

Reduced 0 0.0%

	Annual Costs	(\$/yr)			Chemical C	ost (\$/yr)		
Tank	Disposal	Water	Sewer	RO System			All	Total
					Clep 83M	Defoam		
1	0.00	32.90	8,75	88.83	2,565.00	390.00	2,955.00	\$3,085.48
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	\$0.00
					Caustic	Acid		
3	0.00	300.00	750.00	810.00	190.00	3.23	193,23	\$2,053.23
					Clepo 30B	Acid		
4	0.00	28.80	30.00	77.76	2,108.22	1,415.50	3,523.72	\$3,660.28
5	0.00	18.00	2,295.00	48.60	190.00	3.23	193.23	\$2,554.83
6	0.00	918.00	45.00	2,478.60	95,00	1.62	96.62	\$3,538.22
					Clepo 503			
7	6,040.00	4.00	0.00	10.80	2,789.20		2,789.20	\$8,844.00
					Caustic	Acid		
8	0.00	18.00	3,045.00	48.60	190.00	3.23	193.23	\$3,304.83
					Acid	Pik Aid	,	
9	1,245.00	9.74	0.00	26.30	791.41	0.00	791.41	\$2,072.45
10	14,715.00	0.00	0.00	0.00	15,022.66	7,362.56	22,385.22	\$37,100.22
					Caustic	Acid		
11	0.00	18.00	45.00	48.60	95.00	1.62	96.62	\$208.22
12	0.00	1,218.00	45.00	3,288.60	95.00	1.62	96.62	\$4,648.22
					Iridite	Nitric		
13	1,005.00	0.50	0.00	1.35	462.00	200.00	662.00	\$1,668.85
14	2,010.00	1.00	0.00	2.70	3,150.00	200.00	3,350.00	\$5,363.70
					Caustic	Acid		
15	0.00	300.00	750.00	810.00	190.00	3.23	193.23	\$2,053.23
15	0.00	20 60	45 00	03 62	05.00	1 67	06.63	\$75A 8A

New Costs

Totals	Disposal	Water Sewer DI System	Chemicals	Total
All	\$25,015.00	\$2,897.54 \$7,058.75 \$7,823.36	\$37,615.95	\$80,410.60
Rinse	\$0.00	\$2,820.60 \$7,020.00 \$7,615.62	\$1,159.40	\$18,615.62
%Rinse	0.0%	97.3% 99.5% 97.3%	3.1%	23.2%

Old Costs

Totals	Disposal	Water Sewer RO System	Chemicals	Total
Ali	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
%Rinse	0.0%	98.4% 99.7% 98.1%	4.1%	31.6%

Savings

aringo_						
Totals	Disposal	Water	Sewer	RO System	Chemicals	Total
All	\$0.00	\$1,926.00	\$4,815.00	\$2,867.40	\$383.22	\$9,991.62
Rinse	\$0.00	\$1,926.00	\$4,815.00	\$2,867.40	\$383.22	\$9,991.62

cutting the 654 2 caseade by 40% assuming 4000 hr/gr reduces water by 720,000 gph 2390 gpd 10 mits

Table V-6, include Tank 15 in Cascade 2: Annual savings and waste water reduction for the rinse tanks alone and for all of the tanks. Savings just for adding tank 15 are found by subtracting the values from table V-5

	(gai/hr)	(gal/hr)		Water (gal/vr)				Price Date (Start)			
Tani	Evaporatio	on Flow	Generati	on Evaporat	ion Usage	Diener	Price Dat	a (\$/gal)			
1	3.5		3 500	29.400	32 900	2011/12					
2			1	~ 2000).0027	
3	a k vejnad	- 1 70.5	1 300.00	B. N. S. C. C. S.	No para	18.2.					
4	2		1 3 U U	16,800	1 27.70			<u></u>	<u>an an a</u>	<u>and a strate store</u>	
5		<u> </u>	1 018 00	Part Carl	alarin televisiona an						
6				ter i successive	and the second sec	alexia da esta	n in the second seco	and the state of the	6 6	The second s	
	an a		4,000		000	<u> </u>		<u></u> 1	3, 2000	200	
0	1977 - Antonio Salati Antonio Salati Antonio Salati Antonio Salati Antonio Salati Antonio Salati Antonio Salati Antonio Salati Antonio	المالية (يطرق أيكرز الم	dd e <u>1</u> - Salancessaer	A marin de	<u>. 1920 - 1</u>	an service a service of service of the service of t	N N	tingin (1997)		
	- <u> </u>		<u>i 000</u>	<u> </u>	9,1441	an air an	1	16.11	0001	000	
30 14	i i i i i i i i i i i i i i i i i i i	i Serie associtieres	4.000) 9	The second	- 		مىر بور يې د . مىرىد ئوس ب ې د بې د .			
12	e di serijanjer	es p =	1 8000	n. 1 1988 - 19890 - 1989 - 1989 - 1989 - 1989 - 1989 - 1989 - 1989 - 1989	a service		-				
13		1	500	1	=\\\\\\						
14		1	1 000	1	for :						
15	e en source and an	sele seanes	and the second			and the second sec		and an orall of the local data			
16	- 4 -	SCARE DESIGNATION			State -	And a state	the second	- 1894 All Annual Annual	Second Jaco	and Artic Parts	
	Total	New	2,002,00	0 30,340	لاجتارت و مرک	1	7			er en forste de la comme de La comme de la c	
	gai/yr	Original	4,760,000	0 68,040	4,823,540		/				
	ν.	Reduced	d 2,208,00	0 0	2,208,000		/				
			46.4%	0.0%	45.8%						
	Water	New	2.541.50	68 040	2 600 300	. Х					
		Original	4 749 500	0 68 040	4 808 300						
		Reduced	1 2.208.000) 0	2 202 000	- /	/				
			46.5%	0.0%	45 G%	1					
	Hazardarra	. N	40 505	0.075		/					
	nazargous	s new	10,500			/					
		<u>Original</u>	10,500			/					
		Reduced									
			0.0%			/					
	Annual Cos	ts(Shur)			A de average de la			<u> </u>	-		
Tank	Disposal	Water	Sawar	EO Sictor	- inemical y	COST (SAVE)			-;		
		mater	Jewei	1 U OVSLEI			1 (1) • • • • • • • • • • • • • • • • • • •		, 		
1	0.00	32.90	9.75		2 585 40	<u> </u>			4		
2	0.00	0.00	0.00	1 200	2,000.20	<u></u>		- afric v	L		
		0.00			- 0.00	<u> </u>	<u> </u>	<u> </u>	1		
3.	0.00	300.00	Tourne		- Coustio		estative t				
				1	Ciedo 30B	Acid	i territori i constructione di constructi di constructione di constructione di constructione di construction				
4	0.00	28,80	30.00	1 77.76	1 2.108.22	1,415,50	1 3 573		i		
5	0.00	18.00	2295.00	48.60	anna lanna		States of the second	त्र मार्ग्स स्वयं	5		
6	0.00	918.00	45:00	478.60	a jas and	in the second second	Carlor Pratice	antina na serie de la serie La serie de la s	1		
				1	1 1 lepo 502				1		
/	6,040.00	4.00	0.00	10.80	2,789.20		2.70.41		1		
8	0.00	10.00			Cauatio	<u></u>					
and a contract of	0.00	10:00	Maria Maria	ાં નવે.પ્રયુક્તિ	ficture	Mill WL 34	and the second second	<u> </u>	i \		
9	1 245 00	9.74	1.10	1 26 30	ACIO	PIK AIQ			4 \		
10	14,715.00	0.00	100	1 20.30	191.41	0.00	/51.41	32.572.5	! \		
				1 0.00	1 Caustic	1.002.00 Aria		+ 557 HELV2	· \		
, 11	0.00	18.00	45,00	48.60	95 00		Sectors and		i \		
12	0.00	18.00	45.00	108 80	1 95.00	1000000		The second second second	F E		
				1	Iridite	Nitrin					
13	1,005.00	0.50	0.00	1.25	462.00	200.00	332.33	1 31.0333			
14	2,010.00	1.00	0.00	2.70/	3,150.00	200.00	1 0,000.00				
and the start of				/	Caustic	Acid					
16	0.00	5218.00	70.00	<u>مان،دني</u>	te lou in	Joger -	1000 100 Lan	18- urter	,		
		J. JU.OU	and the second second	ورد المعنى بنكاف المعالية	المحققين الم	્યાસ્ટ ્યાઝ કરવા	n gián na chu a gu	10			
	New Cost										
	new cosis	Disposal	IAL-A-	e							
	A 11	\$25 045 00	C) 645 5 4	Jewer	DI SYSTEM		Chemicals	Total			
	All Sinco	en on	AC.CIO.24	30.000/0	57 051 96		1.537 815 05	1 070 687 10 I			
	«Pine»	<u>μου.υυ</u> Δ Ωον	07:40	STATES OF ADDRESS OF A	N 0 X 4 73		\$1 150				
	/orxi115@	0.0%	36,174	19:0%	AU174		3.1%	21.491			
	Old Coste										
	Totale	Disposal	Water	Chur	80 0		0				
	AII	\$26 015 00	A CONTRACT	JEWBL	nu system		Chemicals	Total			
	All Ding-	<u>a∠0,015.00</u>	<u> ⊅*,3∠3.04</u>	1.31 FOX3/3	310,690.76		537,999	\$90.4-22			
	Maine-		1-04-140:0U	00.000	+ IU,483.02		\$1,542.62	\$28,6074 1			
	76rt11150	0.0%	30.4%		98.1%		4.1%	31 6%			
	Savinar										
	Javings	Disposal	Matar	Course	BO Contract		· · · · · · · · · · · · · · · · · · ·				
	i Utais	e0.00	wrater	Sewer	RU System		Chemicals	Total			
	Binge		⇒∠,∠∪8.00	30,520.00	\$3,628.80		\$383.22	\$11,740.02			
	Rinse	U.UU	⇒2,208.00	\$5,520.00	\$3,628.80		\$383.22	\$11,740.02			

Table V-6, include Tank 15 in Cascade 2: Annual savings and waste water reduction for the rinse tanks alone and for all of the tanks. Savings just for adding tank 15 are found by subtracting the values from table V-5

	(gal/hr)		Water (gally	r)			Bries Data (final)			
Tank	Evanoration	Flow	Generation	Evaporation	lisana	Disposal	Dienocal	Water	Sower	PO Sustam
4	25		0 coo		- Oblige	Disposal	Disposal	Trates	Jewei	NO System
1	3.0		3,500	29,400	32,900	sewer	0.00	0.001	0.0025	0.0027
2							0.00	0.001	0.0025	0.0027
3	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	70.5	300,000		300,000	sewer	0.00	0.001	0.0025	0.0027
4	2		12,000	16,800	28,800	sewer	0.00	0.001	0.0025	0.0027
5		450	918,000	A. 16. 1		sewer	0.00	0.001	0.0025	0.0027
6	and the second second	0	18,000		918,000	sewer	0.00	0.001	0.0025	0.0027
7			4,000		4,000	RCRA	1.51	0.001	0.0000	0.0027
8 .		600	1,218,000	1. S.	18,000	sewer	0.00	0.001	0.0025	0.0027
9	1.1		500	9,240	9,740	RCRA	2.49	0.001	0.0000	0.0027
10			4,500		0	RCRA	3.27	0.001	0.0000	0.0027
		0	18,000		18,000	sewer	0.00	0.001	0.0025	0.0027
12		0	18,000		18,000	sewer	0.00	0.001	0.0025	0.0027
13	$\mathcal{L}^{(1)}$		500		500	RCRA	2.01	0.001	0.0000	0.0027
14	à*		1,000		1,000	RCRA	2.01	0.001	0.0000	0.0027
15		0	18,000		1,218,000	sewer	0.00	0.001	0.0025	0.0027
16	1.5	· 0 ·	18,000	12,600	30,600	sewer	0.00	0.001	0.0025	0.0027

Total	New	2,552,000	68,040	2,615,540
gal/yr	Original	4,760,000	68,040	4,823,540
	Reduced	2,208,000	0	2,208,000
		46.4%	0.0%	45.8%
Water	New	2,541,500	68,040	2,600,300
	Original	4,749,500	68,040	4,808,300
	Reduced	2,208,000	0	2,208,000
		46.5%	0.0%	45.9%
Hazardous	New	10,500		
	Original	10,500		
	Reduced	0		
		0.0%		

	Annual Costs	s(\$/yr)	-		Chemical C	ost (\$/yr)		
Tank	Disposal	Water	Sewer	RO System			All	Total
	Ъ.			1	Clep 83M	Defoam		
1	J 0.00	32.90	8.75	88.83	2,565.00	390.00	2,955.00	\$3,085,48
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	\$0.00
	$\mathcal{A}_{\underline{\lambda}}^{(1)}(t)$				Caustic	Acid		
3	0.00	300.00	750.00	810.00	190.00	3.23.	193.23	\$2,053.23
					Clepo 30B	Acid		
. 4	0.00	28.80	30.00	77.76	2,108.22	1,415.50	3,523.72	\$3,660.28
5	0.00	18.00	2,295.00	48.60	190.00	3.23	193.23	\$2,554.83
6	0.00	918.00	45.00	2,478.60	95.00	1.62	96.62	\$3,538.22
121 					Clepo 503		1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	
7	6,040.00	4.00	0.00	10.80	2,789.20		2,789.20	\$8,844.00
-					Caustic	Acid		
8	0.00	18.00	3,045.00	48.60	190.00	323	193.23	\$3,304.83
					Acid	Pik Aid		
9	1,245.00	9.74	0.00	26.30	791.41	0.00	791.41	\$2,072.45
10	14,715.00	0.00	0.00	0.00	15,022.66	7,362.56	22,385.22	\$37,100.22
					Caustic	Acid		
11		18.00	45.00	48 60	95,00	1.62	96.62	\$208.22
12	0.00	18.00	45.00	48.60	95.00	1.62	96.62	\$208.22
		1			Iridite	Nitric		
13	1,005.00	0.50	0.00	1.35	462.00	200.00	662.00	\$1,668.85
14	2,010.00	1.00	0.00	2.70	3,150.00	200.00	3,350.00	\$5,363.70
					Caustic	Acid		
. 15	0.00	1,218.00	45.00	3,288.60	190.00	3.23	193.23	\$4,744.83
- 16	0.00	30 60	45.00	82 62	95.00	1.62	96.62	875A 8A

New Costs

Totals	Disposal	Water Sewer DI System	Chemicals	Total
Ali	\$25,015.00	\$2,615.54 \$6,353.75 \$7,061.96	\$37,615.95	\$78,662.20
Rinse	\$0.00	\$2,538.60 \$6,315.00 \$6,854.22	\$1,159.40	\$16,867.22
%Rinse	0.0%	97.1% 99.4% 97.1%	3.1%	21.4%

Old Costs

Totals	Disposal	Water Sewer RO System	Chemicals	Total
All	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
%Rinse	0.0%	98.4% 99.7% 98.1%	4.1%	31.6%

Savings

Totals	Disposal	Water	Sewer	RO System	Chemicals	Total
Ali	\$0.00	\$2,208.00	\$5,520.00	\$3,628.80	\$383.22	\$11,740.02
Rinse	\$0.00	\$2,208.00	\$5,520.00	\$3,628.80	\$383.22	\$11,740.02

Table V-5, Cascade 2:
ppublic springs and words words methodian fantha since table sizes and fan die fur

	(gal/hr)		Water (gal/y	/ r)			Price Data	(S/gai)	1	
Tank	Evaporation	Flow	Generation	Evaporatio	n Usage	Disposal	Disposal	Water	Sewer	RO System
1	3.5		3,500	29,400	22,020				. Annu S	1.11
2			1	1	1		+			10027
3	New Contraction of	70 5	10 ann	BARRE, STREES, I		No. 1 and a construction of the	<u>।</u> আজ্যা নার মুরুরে	160.00		
4	2		1 12 000	16 200	1 00 27		سيت يشتح مست	<u>ب منتشکار با است</u>	free to the second	
5	Maria and an		Contra Contra	PERSONAL ST	also de la			The second	and the second secon	
6	State States and States 7	Statistica and the state	1 anon	Same of the State	a the second second				A service of the serv	100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100
7	1		1.000		V	an a	<u>ar an an an an an an an</u>	<u>interes de la Antoire</u>	and a second	، <u>مانت</u> قانات، المتعانينية، الرواب الم
8	Maghale general a share	~~~~	Product State	har and a second		an a gan an Alban Alban		the second second		Here and the second
9	i.1	<u> </u>	1 300		1 a.c.		n a la <u>stran</u> tai			
10	1		4.500		1		· · · · · · · · · · · · · · · · · · ·		1 10	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
11	ALCONDUCTION OF	SALE OF COMPANY	NOT BULLIN	Parente and a second	MIROS NH	and and a state of the second se		Letter and a second	್ರಾ	an an traditional an An traditional an trad
12	Attended and the	estable Otocore	10001842A	Contraction of the second	SHEEKS .	1. A. A.	an a		an in the state of	
13	i		1 500	{	1 500	na in an an an an an An An A	لك الدراب المحموس	te i se se se	1000	3977
14			1 1,000	i	TIN					
15	Lingerstyre i	70.5	300 10	no ana sario (Alexan \		िक स्टब्स मुख्य	Section 1978	and the second	and Contraction
16	15	0	18 0.47	17/10/01	- see see	1. sp. 1	• ***** / ***	i a a a a a a a a a a a a a a a a a a a	2011 - C-19	and the second s
	Total	Jaw	2.324.300	32.040		1				
	solba	Original	1 780 000	80.000		1	. /.			

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Water	New	2,823,500	68,040	2.882.300	
	Keduced	1, 926,000 40.5%	0 0.0%	1,926,000 \ 39.9%	١
				102010101	

				£,00£,000
	Original	4,749,500	68,040	4,808,300
• •	Reduced	1,926,000 40.6%	0 0.0%	1,926,000 40,1%
Hazardous	New	10,500		
	Original	10,500		
	Reduced	0		

Reduced 0 0.0%

.

	Annual Cost	s(\$/yr)			Chamicui C	Just wight			
Tank	Disposal	Water	Sawar	RO Syster	1	1		4 . Sta	i
			1		1 Ciep 63M	/ erca			1
1	0.00	32.90	d.75	33.33	2,565.00	390.00	1 1.800 1	1.5	
2	0.00	0.00	0,00	0.00	1 0.00 /	1.0.00		1	1
			i		I Caustig	Acia	T	•	. 1
3	0.00	300.00	750 0	810.00	150.00	10000 32 2	1 + d	6. S. S.	1 201
			ł.		Clebo 103	1 JOIN]
	0.00	28.80	30 00	77.79	2.109.22	1 1 1195 5	1 - 2 - 2 - 1	~	0
5	0.00	18:00	2005 AA	in the second	+0000	Assertion of the	100	en ang ang a	1.2.1
6	0.00	918.00	and the second	**************************************	ind un	1980 - 14 2-4 7		ده میرون یمی د اینیا این محمد بید	
					1 Clarla 300			1	·
7	6,040.00	4.00	0.00	10.00	2,700.20	1	· · · · · · · · · · · · · · · · · · ·	Line .	
				·	Chustic	ંનંદત્વ	1.	1	;
8	0.00	18.00	× 3,0+53		p build	Kaile -	in an	and the second second	1.486
					Acia	L Pik Aic	1		1
9	1,245.00	9.74	0.00	26,30	1 791.41	0.00	791	52.	-5 I
10	14,715.00	0.00	0.00	0.00	15,022,66	1 7,362.55	12.18c 1	: 37 🔪	22
					Caustic	Acid			
<u>11</u>	0.00	18.00	45.00	48.60	95.00	1.52		<u> </u>	1000
12	0.00	1,218.00	200 AS / 10	ં ઉત્તરમ કંપે	See 95 not	0%% + 8 ?			12
					'ridite	Alitro			∇
13	1,005.00	0.50	0.00	1 35	452.00	200.00	2.00		7
14	2,010.00	1.00	0.00	2.70	2,150.00	200.00			3
					Caustic	A010			! '
15	0.00	300.00	ار (۲۰ <mark>۰۵) پخریدی زمونیده ۲۰۰۵ (</mark> ۲۰۰۱) د در مانیک افکار فکار میکانید در ۲۰۰۱ (۲۰۰۱)	a ser a Ser a ser	160.00	in and a	and a second	a por en antenar	
16	0.00	30.60	45.00	82.62	95.00	1.62	96.62	\$254.8	4

New Costs

Totals	Disposal	Water Sewer DL System	Caemic us i	ice i
All	\$25,015.00	\$2,897.54 \$7,058.75 \$7,823.36	\$37,615.95	\$80,410.60
Rinse	\$0.00	\$2,820.60 \$7,020.00 \$7,615.62	\$1,159.40	\$18,615.62
%Rinse	0.0%	97.3% 99.5% 97.3%	3 1%	23.2%

Old Costs

10 00313				
Totals	Disposal	Water Saure BO Suctor	Chamicain I	T-
Ati	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
%Rinse	0.0%	98.4% <u>39.7%</u> 98.1%	4,170	31.0%

Savings

Totals	Disposal	Water	Sewer	RO System	Chemicais	l'otal
All	\$0.00	\$1,926.00	\$4,815.00	\$2,867.40	\$383.22	\$9,991.62
Rinse	\$0.00	\$1,926.00	\$4,815.00	\$2,867.40	\$383.22	\$9,991.62

Table V-7, Cascade Tank 16 and Tank 15: Values are shown for the rinse tanks alone and for all of the tanks.

	(gal/hr)		Water (gal/y	ı r)			Price Data (\$/gal)		
Tank	Evaporation	Flow	Generation	Evaporation	Usage	Disposal	Disposal	Water	Sewer	RO System
1	3.5		3,500	29,400	32,900	sewer	0.00	0.001	0.0025	0.0027
2							0.00	0.001	0.0025	0.0027
3		70.5	300,000		300,000	sewer	0.00	0.001	0.0025	0.0027
4	2		12,000	16,800	28,800	sewer	0.00	0.001	0.0025	0.0027
5		450	918,000		18,000	sewer	0.00	0:001	0.0025	0.0027
6		0	18,000		918,000	sewer	0.00	0.001	0.0025	0.0027
7	N 1 2		4,000		4,000	RCRA	1.51	0.001	0.0000	0.0027
8		540	1,098,000		1,098,000	sewer	0.00	0.001	0.0025	0.0027
9	- 1.1		500	9,240	9,740	RCRA	2.49	0.001	0.0000	0.0027
10			4,500		0	RCRA	3.27	0.001	0.0000	0.0027
11		211.5	864,000		864,000	sewer	0.00	0.001	0.0025	0.0000
12		600	1,218,000		1,218,000	sewer	0.00	0.001	0.0025	0.0027
13			500		500	RCRA	2.01	0.001	0.0000	0.0027
14	S		1,000		1,000	RCRA	2.01	0.001	0.0000	0.0027
15		70.5	300,000		18,000	sewer	0.00	0.001	0.0025	0.0027
16	1.5	0	18,000	12,600	312,600	sewer	0.00	0.001	0.0025	0.0027

	Provide the second state of the second stat	A stability of the s	ACCORDING AND A CARDINATION CONTRACTOR	the Charles Construction of the Charles of the Char	877.X
Total	New	4,760,000	68,040	4,823,540	
gai/yr	Original	4,760,000	68,040	4,823,540	
	Reduced	0	0	0	
		0.0%	0.0%	0.0%	
Water	New	4,749,500	68,040	4,808,300	
	Original	4,749,500	68,040	4,808,300	
	Reduced	0	0	0	
		0.0%	0.0%	0.0%	
Hazardous	New	10,500			
	Original	10,500			
	Reduced	0			
		0.0%			

N.2	Annual Costs	(\$/уг)			Chemical C			
Tank	Disposal	Water	Sewer	RO System			All	Total
	-24				Alkaline	Defoam		
1	0.00	32.90	8.75	88.83	2,565.00	390.00	2,955.00	\$3,085.48
2	- 0.00	0.00	0.00	0.00	0.00	0.00	0.00	\$0.00
					Caustic	Acid		
3	0.00	300.00	750.00	810.00	190.00	3.23	193.23	\$2,053.23
: 			· ·		Etch	Acid		
4	0.00	28.80	30.00	77.76	2,108.22	1,415.50	3,523.72	\$3,660.28
					Caustic	Acid		
5	0.00	18.00	2,295.00	48.60	190,00	3,23	193.23	\$2,554.83
6	0.00	918.00	45.00	2,478.60	95.00	1.62	96.62	\$3,538.22
and .					Deox			
7	6,040.00	4.00	0.00	10.80	2,789.20		2,789.20	\$8,844.00
					Caustic	Acid		
8	0.00	1,098.00	2,745.00	2,964.60	190.00	3.23	193.23	\$7,000.83
					Acid	Pik Aid		
. 9	1,245.00	9.74	0.00	26.30	791.41	0.00	791.41	\$2,072.45
10	14,715.00	0.00	0.00	0.00	15,022.66	7,362.56	22,385.22	\$37,100.22
					Caustic	Acid		
11	0.00	864.00	2,160.00	0.00	380.00	3.23	383.23	\$3,407.23
12	0.00	1,218.00	3,045.00	3,288.60	190,00	3.23	193,23	\$7,744.83
					Iridite	Nitric		
13	1,005.00	0.50	0.00	1.35	462.00	200.00	662.00	\$1,668.85
14	2,010.00	1.00	0.00	2.70	3,150.00	200.00	3,350.00	\$5,363.70
					Caustic	Acid		
15	0.00	18.00	750.00	48.60	190.00	3.23	193.23	\$1,009.83
16	0.00	312.60	45 00	844.02	95.00	1.62	96.62	\$1 298 24

New Costs ____

Totals	Disposal	Water Sewer RO System	Chemicals	Total
IIA	\$25,015.00	\$4,823,54 \$11,873,75 \$10,690,76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
%Rinse	0.0%	98.4% 99.7% 98.1%	4.1%	31.6%

Old Costs

14 00000				
Totals	Disposal	Water Sewer RO System	Chemicals	Total
Ali	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
%Rinse	0.0%	98.4% 99.7% 98.1%	4.1%	31.6%

Savings

Totals	Disposal	Water	Sewer	RO System	Chemicals	Total
All	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00
Rinse	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00

Table V-8, tanks are Cleaned Less Often (Half as Much) Values are for the rinse tanks alone and for all of the tanks.

concentration

	(gal/hr) Water (gal/yr)						Price Data (\$/gal)			
Tank	Evaporation	Flow	Generation	Evaporation	Usage	Disposal	Disposal	Water	Sewer	RO System
1	3.5		3,500	29,400	32,900	sewer	0.00	0.001	0.0025	0.0027
2						0		0.001	0.0025	0.0027
3		70,5	291,000		291,000	sewer	0.00	0.001	.0.0025	0.0027
4	2		12,000	16,800	28,800	sewer	0.00	0.001	0.0025	0.0027
5		450	909,000		9,000	sewer	0.00	0.001	0.0025	0.0027
6		0	9,000		909,000	Sewer	0.00	0.001	0.0025	0.0027
7			4,000		4,000	RCRA	1.51	0.001	0.0000	0.0027
8	and the second second	540	1,089,000		1,089,000	Sewer	0.00	0.001	0.0025	0.0027
9	1.1		500	9,240	9,740	RCRA	2.49	0.001	0.0000	0.0027
10			4,500		0	RCRA	3.27	0.001	0.0000	0.0027
41		211.5	855,000		855,000	sewer	0.00	0.001	0.0026	0.0000
12		600	1,209,000		1.209.000	sewer	0.00	0.001	0.0025	0.0027
13			500		500	RCRA	2.01	0.001	0.0000	0.0027
14			1,000		1,000	RCRA	2.01	0.001	0.0000	0.0027
15		70,5	291,000		291,000	sewer	0.00	0.001	0.0025	0.0027
16	1.5	0	9,000	12,600	21,600	sewer	0.00	0.001	0.0025	0.0027

Water	New	4,677,500	68,040	4,736,300
		1.5%	0.0%	1.5%
	Reduced	72,000	0	72,000
gal/yr	Original	4,760,000	68,040	4,823,540
Total	New	4,688,000	68,040	4,751,540
- L .C		3,000	12,000	21,000

	144.11	4,077,000	00,040	
	Original	4,749,500	68,040	4,808,300
	Reduced	72,000	0	72,000
		1.5%	0.0%	1.5%
Hazardous	New	10,500		
	Original	10,500		
	Reduced	0		

0.0%

	Annual Costs	(\$/yr)			Chemical Cost (\$/yr)			
Tank	Disposal	Water	Sewer	RO System			All	Total
					Clep 83M	Defoam		
1	0.00	32.90	8.75	88.83	2,565.00	390.00	2,955.00	\$3,085.48
2	0.00	0.00	0.00	0.00			0.00	\$0.00
					Caustic	Acid		
3	0.00	291.00	727.50	785.70	142.50	2.60	145.10	\$1,949.30
					Clepo 30B	Acid		
4	0.00	28.80	30.00	77.76	2,108.22	1,415.50	3,523.72	\$3,660.28
					Caustic	Acid		
5	0.00	9.00	2,272.50	24.30	142.50	2.60	145.10	\$2,450.90
6	0.00	909:00	22.50	2,454,30	95.00	0.63	95.63	\$3,481.43
					Clepo 503			
7	6,040.00	4.00	0.00	10.80	2,789.20		2,789.20	\$8,844.00
					Caustic	Acid		
8	0,00	1,089.00	2,722.50	2,940.30	142.50	2.60	145.10	\$6,896.90
				1	Acid	Pik Aid		
9	1,245.00	9.74	0.00	26.30	791.41	0.00	791.41	\$2,072.45
10	14,715.00	0.00	0.00	0.00	15,022.66	7,362.56	22,385.22	\$37,100.22
					Caustic	Acid		
11	0.00	855.00	2,137.50	0.00	213.75	2.60	216.35	\$3,208.85
12	0.00	1,209.00	3,022.50	3,264.30	142.50	2.60	145.10	\$7,640.90
					Iridite	Nitric		
13	1,005.00	0.50	0.00	1.35	462.00	200.00	662.00	\$1,668.85
14	2,010.00	1.00	0.00	2.70	3,150.00	200.00	3,350.00	\$5,363.70
					Caustic	Acid		
15	0.00	291.00	727.60	785.70	142.50	2.60	145.10	\$1,949.30
16	0.00	21.60	22.50	58.32	47.50	0.63	48.13	\$150.55

New Costs

Totals	Disposal	Water Sewer RO System	Chemicals	Total
All	\$25,015.00	\$4,761.54 \$11,693.75 \$10,520.66	\$37,542.16	\$89,523,11
Rinse	\$0.00	\$4,574.60 \$11,655.00 \$10,312.92	\$1,085.61	\$27,728.13
%Rinse	0.0%	98.4% 99.7% 98.0%	2.9%	31.0%

Old Costs

in ovala			· · · · · · · · · · · · · · · · · · ·	
Totals	Disposal	Water Sewer RO System	Chemicals	Total
All	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402,22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.62	\$28,607.24
%Rinse	0.0%	98.4% 99.7% 98.1%	4.1%	31.6%

Savings

aringe.						
Totals	Disposal	Water	Sewer	RO System	Chemicals	Total
All	\$0.00	\$72.00	\$180.00	\$170.10	\$457.01	\$879.11
Rinse	\$0.00	\$72.00	\$180.00	\$170.10	\$457.01	\$879.11
•						

Table V-7, Cascade Tank 16 and Tank 15: Values are shown for the rinse tanks alone and for all of the tanks.

		Water (gai/yr)				Price Data (\$/gal)			
Evaporation	Flow	Generation	Evaporation	Usage	Disposal	Disposal	Water	Sewer	RO System
3.5		3,500	29,400	32,900	sewer	0.00	0.001	0.0025	0.0027
		1			l	0.00	2.001	0.0005	0.0007
Sec.	705	1 300 000	i s and and	athe wares	Kalenda, San Jawa	Sector Sector	Server State	The second second	3027
2		12,000	16.8/_0	<u>28 0 0</u>	71/01	0.30	1 0 00 1	1 775	2027
and a second	-factories	A TATY	lette installigende		and the second sec	Carry Carry	and the second secon	ATTACK AND THE PARTY	1000 C 1000-000
ter in the second second	A CARLES	les concers	NAS AND AND A DESCRIPTION	78.6	and a second sec		بر میں ایک ک ی کر ایک کر کر ایک کر کر ایک کر کر ایک کر کر ایک میں کر	and a state of the second s	
		1,000		1.000					and the second
And Andrews		and the second s	ar an ann an	n and a second	- Strand		e parte production de la companya de La companya de la comp	and the second secon	
1.1		ÚÚČ I	j 3,240 j		n an	1		in the second	و، استیت ایک از در مشتخصی از ایران
		4.500	1	na n	an a	and the second sec	an an an tri		
	115	18 34 1008		APR 1. 57(3.4.	1. A. M. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	and officer	and the second	anis - Anis -	esteral de la
and the second	SCROOL	Pin	States 1	On P		a far a s		and the second s	
1		- 22	1	FC			· · · · · · · · · · · · · · · · · · ·		
		1,000		1.000		1			
	aller and an area and a second	All and a second to		S Production		7			بالمحمد الأثبات المحمد
and a company	antes de la compañía	Parties and a second state	Enter	i ananani.		fain 200 that a	n dining the second	and a state of the second s	anter anteraria
Total	New	4. /60.000	3 040	1.323 5.43			and an	and the second	na seren en e
ααί/ντ	Criginal	4 760.0 30	38 040	4 823 540					
	Reduced	0	0	0	· /				
		0.0%	0.0%	0.0%					·
		0.076	0.070	0.070	· /				
Water	New	4,749,500	68,040	4,808,300					
	2 1 3.5 2 1.1 1.1 1.1 1.1 1.1 1.1 1.1	2 Prove 2 Prove 2 Prove 2 Prove 1.1 1.1 211:52 FIG FIG FIG FIG FIG FIG FIG FIG	Evaporation Flow Generation 3.5 3,500 2 12,000 1.1 1,000 2 12,000 1.1 1,000 2 1,000 2 1,000 2 1,000 2 1,000 2 1,000 2 1,000 2 1,000 2 200 2 <td>Evaporation Flow Generation Evaporation 3.5 3,500 29,400 29,400 2 12,000 16,8/ 29,400 2 12,000 16,8/ 200,000 3.5 3,500 29,400 36,8/ 2 12,000 16,8/ 36,000 3.5 3,500 29,400 36,000 3.5 3,500 29,400 36,000 3.5 3,500 34,000 36,040 1.1 1,500 37,000 36,040 1.1 1,000 36,040 39,040 1.1 1,000 38,040 0,00%</td> <td>Evaporation Piow Generation Evaporation Usage 3.5 3,500 29,400 32,900 2 12,000 16,80 28,000 2 12,000 16,80 28,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,040 4,323,540 1.000 1,000 3,040 4,323,540 1.000 0 0 0 1.000 0,00% 0,0% 0,0% 1.000 0,00% 0,0% 0,0%</td> <td>Evaporation Piow Generation Evaporation Usage Disposal 3.5 3,500 29,400 32,900 sewer 2 12,000 16,87 28,77 16,87 28,77 1 12,000 16,87 28,77 16,87 28,77 16,87 1 12,000 16,87 28,77 16,97 16,97 16,97 1 1,000 3,240 9 16,97 16,97 16,97 16,97 1.1 1 300 3,240 9 16,97</td> <td>Evaporation Piow Generation Evaporation Usage Disposal <thdisposal< th=""></thdisposal<></td> <td>Evaporation Piow Generation (Evaporation) Usage Disposal Disposal Water 3.5 3.500 29,400 32,900 sewer 0.00 0.001 2 12,000 16,87 280,000 sewer 1.000 3.000 2 10,000 3,240 9 2.000 1.000</td> <td>Evaporation Flow Generation Evaporation Usage Disposal Water Sewer 3.5 3.500 29.400 32.900 sewer 0.00 0.001 0.0025 2 12.000 16.87 28.0 200 <t< td=""></t<></td>	Evaporation Flow Generation Evaporation 3.5 3,500 29,400 29,400 2 12,000 16,8/ 29,400 2 12,000 16,8/ 200,000 3.5 3,500 29,400 36,8/ 2 12,000 16,8/ 36,000 3.5 3,500 29,400 36,000 3.5 3,500 29,400 36,000 3.5 3,500 34,000 36,040 1.1 1,500 37,000 36,040 1.1 1,000 36,040 39,040 1.1 1,000 38,040 0,00%	Evaporation Piow Generation Evaporation Usage 3.5 3,500 29,400 32,900 2 12,000 16,80 28,000 2 12,000 16,80 28,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,240 3,000 1.1 1,000 3,040 4,323,540 1.000 1,000 3,040 4,323,540 1.000 0 0 0 1.000 0,00% 0,0% 0,0% 1.000 0,00% 0,0% 0,0%	Evaporation Piow Generation Evaporation Usage Disposal 3.5 3,500 29,400 32,900 sewer 2 12,000 16,87 28,77 16,87 28,77 1 12,000 16,87 28,77 16,87 28,77 16,87 1 12,000 16,87 28,77 16,97 16,97 16,97 1 1,000 3,240 9 16,97 16,97 16,97 16,97 1.1 1 300 3,240 9 16,97	Evaporation Piow Generation Evaporation Usage Disposal Disposal <thdisposal< th=""></thdisposal<>	Evaporation Piow Generation (Evaporation) Usage Disposal Disposal Water 3.5 3.500 29,400 32,900 sewer 0.00 0.001 2 12,000 16,87 280,000 sewer 1.000 3.000 2 10,000 3,240 9 2.000 1.000	Evaporation Flow Generation Evaporation Usage Disposal Water Sewer 3.5 3.500 29.400 32.900 sewer 0.00 0.001 0.0025 2 12.000 16.87 28.0 200 <t< td=""></t<>

Water	New	4,749,500	68,040	\ 4,808,300	
	Original	4,749,500	68,040	4,808,300	
	Reduced	0	0	\ 0	
		0.0%	0.0%	\Q.0%	
Hazardous	New	10,500			
	Original	10,500			1
	Reduced	0			
		0.0%			1
					1

	Annual Cost	s(\$/yr)			Chemical Cost (\$/vr)			1	
Tank	Disposal	Water	ewer	RC System	i l	Λ	All	ionai	
				1	I Alkaline	menter 1		- in the state of the	
1	0.00	32.90	3.75	18.83	1 1.565.00	1 390.00	2055 191		
2	0.00	0.00	100	1 100	0.00	0,00	0.00	р г	
				1	22112117	A Sector			
3	0.00	300.00	a series	nterior de Arthurado Antonio de Arthurado	Part and and	an and a start	Station and a second		
					Eich	T			
4	0.00	28.80	_0.00	1 7.78	108.12	1,415.50	3,023.12	ە بە ۋىغد	
				1	austic	Acid	1		
5	0.00	18.00	2, 95	8:60	90.40	A MARCH 1866-5	* 198 CT	$\sim \nabla = 0$	
6	0.00	918.00	500	No. or all	10 95 1 100	· · · · · · · · · · · · · · · · · · ·		, en d e se d e se	
					2010	1			
7	6,040.00	4.00	1.00	1.20			2.7.		
-					<u></u>			-	
- 8	0.00	1,098.00	2, 00	And Constant	100 calesonation	C Continues	See 🔪	Sec. 19	
				·		Pik Ald			
9	1,245.00	9.74),00	6.30	91.41	0.00	91		
_10	14,715.00	0.00).00	<u>).00</u>	5.022.66	7 362 56	tin and an	1	
000000000000000000000000000000000000000			Notes and the second	The second second	<u>Jaileti</u> C	<u> </u>			
41	0.00	354.00	2,		and the second second			manifest a loss of	
12	0.00	1,218,00	St nume	and the second	Same and the second second	the second second	and a second		
- 10	4 005 00	0.50		<u> </u>	diale	NIUC		······································	
13	1,005.00	0.50	1.00	<u> </u>	+02.00	<u> </u>	004	un es ser se di	
14	2,010.00	1.00	1.00		1.150.00	200.00	3.350.00		
1159 D		and the second se		1	Jaustic	Acid	l Marine I tarre estate	a Na sana ang mananang manakan	
12	0,00 .		100.00	48,60	190.00	s	193.23	51,009,83	

New Costs

Totais	Disposal	Marca	Chen	70.01
All	\$25,015.00	\$4,823,54 \$11,873,75 \$10,690,76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4,746.60 \$11,835.00 \$10,483.02	\$1,542.52	\$28.607.24
%Rinse	0.0%	914% 917% 381%	4.1%	31,5%

Old Costs

Totals	Disposal	Water Sewer RC System	Chemicals	Total
All	\$25,015.00	\$4,823.54 \$11,873.75 \$10,690.76	\$37,999.17	\$90,402.22
Rinse	\$0.00	\$4 40.00 1 311 aud 100 1, 1, 400.02	31,542.02	⇒∠0,0U/+
%Rinse	0.0%	91.478	4.1%	31.0%

Savings

Totais	Disposal	Water	Sewer	RO System	Chemicals	Total
All	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00
Rinse	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00

want to reduce drag out in cold chem tanks 7,10,13,14 only 2 would be sed in same process o also drain the preceeding muse, the merease = 4×25 = 100 sec (1.7mh) 1.7 mm 22 200 day hr 185 = 19600 / 47 c. Savings from Decreased Carry-Over Volume I tank/Eyde = #4500 / 47 Estimated carry-over volume was calculated and then subtracted from Appendix A the original number. Table V-9 and table V-10 show the annual savings from increased drip-time and from a modified basket design respectively. chromates too-didut Calculations are explained below. Carry over Value 2 tank 1 doal 20 code 200 day 3200 golday of dolvted to recover 2 tank 1 doal 20 code 200 day 3200 golday of dolvted to recover intess waste treedm Calculation Explanation for Carry-Over Volume Reduction if withou is used 10/day Sou of dolvte 100 day of the source the source the gold of concentration In all coses non heated tends experience 400 gold of concentration Corry -over volume Reduction (Tanks 7, 10, 13 and 14) Extend Driplime · 60% of drainable corry-over · for example 100 gallons total congover only half is drainable (50 gallons) (100 - 0.60(50)) gallons = 70 gallons men corry-over Potential Process time increase increase overage of 4 min /aycle. (#85)= 4 min (2004des) (daug) (-1000hor / has cycke (daug) (24ha) (-1000hor / has borne por Abomán 167 day/41 Looked Modification) (20 bookets) (350 deup) = 272.3 gol 0.0389gol booket have 2 operators 270 gollons subtrocted from original volue 25hifts \$0ho/guk = 4000 hr = 200 work days with over these process themenerease = \$ 22,700/gr 4 min 20 cycle 200 wkday FOUND HES cycle duy 57 basket saving .0389 gal 120 basked 200 day = 121,6 gal /m per chemical tank

Table V-9, Increase Drip-Time to reduce Carry-Over Volume: All values listed in the table are annual values.

It was assumed that the drainable carry-over was reduced by 60%.

		Chemical		to charge	time	Extra to reple	Wilsh	Carry-Over		
	Tank	Usage		Changes		Pounds	Ť	(gal)	Price	per
Alkaline	1	2,700	b	2,250	lb	450	lb	900	\$0.95	lb
Etch	4	2,571	b	2,256	lb	315	ib	840	\$0.82	lb
Deoxidizer	7	347	gal	300	gal	47	gai	938	\$7.60	dal
Passivate	9	4,497	b	2,943	lb	1,554	lb	264	\$0.18	b
Nitric	10	75,634	lb	52,965	lb	22,669	lb	1.926	\$0,18	lb
Pik-Aid	10	2,601	lb	1,500	lb	1,101	lb	2.202	\$2.56	ĺb
Clear	13	59	lb	32	lb	27	lb	426	\$6.60	lb
Yellow	14	247	lb	63	ĺb	184	lb	1,472	\$9.00	lb

hat Not

hot

New	Values	

	Annual Costs		
Tank	Changes	Extra	Total Cost
1	\$2,137.50	\$427.50	\$2,565.00
4	\$1,849.92	\$258.30	\$2,108.22
7	\$2,280.00	\$356.44	\$2,636.44
9	\$517.97	\$273.44	\$791.41
10	\$9,321.84	\$3,989.75	\$13,311.59
10	\$3,840.00	\$2,818.56	\$6,658.56
13	\$211.20	\$175.73	\$386.93
14	\$562.50	\$1,656.00	\$2,218.50
Totals	\$20,720.93	\$9,955.71	\$30,676.64

Original Values

	Annual Costs	;	
Tank	Changes	Extra	Total Cost
1	\$2,137.50	\$427.50	\$2,565.00
4	\$1,849.92	\$258.30	\$2,108.22
7	\$2,280.00	\$509.20	\$2,789.20
9	\$517.97	\$273.44	\$791.41
10	\$9,321.84	\$5,700.82	\$15,022.66
10	\$3,840.00	\$3,522.56	\$7,362.56
13	\$211.20	\$250.80	\$462.00
14	\$562.50	\$2,587.50	\$3,150.00
Totals	\$20,720.93	\$13,530.12	\$34,251.05

Savings

Savings				11 to truth
	Annual Savin	igs		1 CONCANNAN
Tank	Changes	Extra	Total	1
1	\$0.00	\$0.00	\$0.00	
4	\$0.00	\$0.00	\$0.00	*******
7	\$0.00	\$152.76	\$152.76	20, lool - 2006
9	\$0.00	\$0.00	\$0.00	
10	\$0.00	\$1,711.07	\$1,711.07	9500 14
10	\$0.00	\$704.00	\$704.00	NOST IN
13	\$0.00	\$75.08	\$75.08	Π.
14	\$0.00	\$931.50	\$931.50	
Totals	\$0.00	\$3,574.41	\$3,574.41	1.20%9

orthric tank \$2411/91 \$9775 (b)ar 67% 9796

Appendix A

poorassumption

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Table V-10, Basket Modification to Reduce Carry-Over Volume: It was assumed that carry-over was only reduced for the non-heated tanks. . Conventors

TankUsageChangesPounds(gal)PriceperAlkaline12,700lb2,250lb450lb900\$0.95lbTable40.574lb2.520lb450lb900\$0.95lb	
Alkaline 1 2,700 lb 2,250 lb 450 lb 900 \$0.95 lb 8%	
$= 100 - 4 - 2,371 - 10 - 2,256 - 10 - 315 - 10 - 840 - $0.82 - 10 - 2,\frac{1}{2}$	
Deoxidizer 7 354 gal 300 gal 54 gal 1,070 \$7.60 gal 7% c	old
Passivate 9 4,497 lb 2,943 lb 1,554 lb 264 \$0.18 lb 40%	* t
Nitric 10 82,178 lb 52,965 lb 29,213 lb 2,482 \$0.18 lb 2020 C	010
Pik-Aid 10 2,741 lb 1,500 lb 1,241 lb 2,482 \$2.56 lb	
Clear 13 53 lb 32 lb 21 lb 338 \$6.60 lb 37	alo
Yellow 14 316 lb 63 lb 254 lb 2,030 \$9.00. lb 36 0	old

New Values

	Annual Costs		
Tank	Changes	Extra	Total Cost
1	\$2,137.50	\$427.50	\$2,565.00
4	\$1,849.92	\$258.30	\$2,108.22
7	\$2,280.00	\$406.60	\$2,686.60
9	\$517.97	\$273.44	\$791.41
10	\$9,321.84	\$5,141.51	\$14,463.35
10	\$3,840.00	\$3,176.96	\$7,016.96
13	\$211.20	\$139.43	\$350.63
14	\$562.50	\$2,283.75	\$2,846.25
Totals	\$20,720.93	\$12,107.49	\$32,828.42

Original Values

	Annual Costs		
Tank	Changes	Extra	Total Cost
1	\$2,137.50	\$427.50	\$2,565.00
4	\$1,849.92	\$258.30	\$2,108.22
7	\$2,280.00	\$509.20	\$2,789.20
9	\$517.97	\$273.44	\$791.41
10	\$9,321.84	\$5,700.82	\$15,022.66
10	\$3,840.00	\$3,522.56	\$7,362.56
13	\$211.20	\$250.80	\$462.00
14	\$562.50	\$2,587.50	\$3,150.00
Totals	\$20,720.93	\$13,530.12	\$34,251.05

Savings

	Annual Savin	gs	
Tank	Changes	Extra	Total
1	\$0.00	\$0.00	\$0.00
4	\$0.00	\$0.00	\$0.00
7	\$0.00	\$102.60	\$102.60
9	\$0.00	\$0.00	\$0.00
10	\$0.00	\$559.31	\$559.31
10	\$0.00	\$345.60	\$345.60
13	\$0.00	\$111.38	\$111.38
14	\$0.00	\$303.75	\$303.75
Totals	\$0.00	\$1,422,63	\$1,422,63

d. Electric Cost for Cascading Tank 16 and Tank 15

Table V-29 in appendix B, section 1-b shows the temperature data used for the following calculation.

$$Q = m (p \Delta T)$$

$$(p = 1 B + u | U \circ F)$$

$$lq lcm3$$

$$453.593q = 1 U \\
28317 cm3 = 7.4805 gal

9.486 × 10-4 B + U = 2.778 × 10-7 K wh

350 dayp / year

 $\Delta T = 4^{\circ}F = 7 (123 - 119)^{\circ}F$ from Temperatur data

$$Q = \left(\frac{500 \text{ got}}{m}\right) \left(\frac{1187 U}{2716}\right) \left(\frac{105}{453.543g}\right) \left(\frac{195}{28317 \text{ cm}^3}\right) (44)$$

 $\Lambda from + arksize.$

$$Q = 16691 \frac{B + U}{hc} \left(2.778 \times 10^{-7} \frac{K w K}{BT u}\right)$$

$$Q = 5 kw$$

 $5 kw \left(\frac{4000 hc}{year}\right) \left(\frac{80.032}{kw k}\right) = \left(\frac{4}{2640} / year\right)$

in electric costs$$
e. Economic Analysis

The calculations for the economic analysis are explained below. Table V-11 shows the economics for Cascade 1, table V-12 shows the economics for Cascade 2, and Table V-13 shows the calculations for including Tank 15 in Cascade 2. Table V-14 shows the economics of purchasing a conductivity meter without considering the annual savings from decreased down-time, while table V-15 shows the economic analysis when down-time is considered.

Explanation of Economic Calculations

NPV = Co +
$$\frac{2}{2}$$
 $\frac{Ci}{(1+r)^{1}}$ Co capital investment
Ci = Savings-t(Savings) r rate of neturn
(assume 15%)
t tax nate
(assume 50%) n life of project
(assume 50%)
DCFRR descounted (ash flow nate of return
let NPV=D let r be the variable
iterate to solve for r
Break Even Point on Paybock Period
make a plot.
NPV

Table V-11, Economic Analysis for Cascade 1:A 50% tax rate was assumed and a 15% rate of return was assumed

		\$85.00		
Savings (\$/year)	Savings (\$/month)	Down Time (\$)	Cascade (\$)	Meter (\$)
1,636.79	136.40	0.00	500.00	0.00
Cash Flow/year	r .	Liners (\$)	Total Cost (\$)	
\$818.40		0.00	500.00	
Year	Payback Time	NPV @15%	r	DCFRR
0	-500.00			
1	211.65	711.65	162.4%	311.93
2	830.48	618.83	162.4%	118.89
3	1,368.59	538.11	162.4%	45.32
4	1,836.51	467.92	162.4%	17.27
5	2,243.40	406.89	162.4%	6.58
	per year	\$2,243.40		\$0.00

	Payback	Time
years		0.69
months		8.26

0.00



Table V-12, Economic Anlysis for Cascade 2: A 50 % tax rate and 15 % rate of return was assumed. hours down price/hour down

nouis down	price/riour down		
5	\$85.00		
Savings (\$/month)	Down Time (\$)	Cascade (\$)	Meter (\$)
832.64	425.00	1,000.00	0.00
	Liners (\$)	Total Cost (\$)	
	4,000.00	5,425.00	
Payback Time	NPV @15%	r	DCFRR
-5,425.00	~		Ŧ
-1,080.82	4,344.18	88.2%	2,654.71
2,696.73	3,777.55	88.2%	1,410.68
5,981.56	3,284.83	88.2%	749.61
8,837.93	2,856.37	88.2%	398.33
11,321.73	2,483.80	88.2%	211.67
per year	\$11,321.73		\$0.00
	5 Savings (\$/month) 832.64 Payback Time -5,425.00 -1,080.82 2,696.73 5,981.56 8,837.93 11,321.73 per year	5 \$85.00 Savings (\$/month) Down Time (\$) 832.64 425.00 Liners (\$) 4,000.00 Payback Time NPV @15% -5,425.00 -1,080.82 -1,080.82 4,344.18 2,696.73 3,777.55 5,981.56 3,284.83 8,837.93 2,856.37 11,321.73 2,483.80 per year \$11,321.73	5 \$85.00 Savings (\$/month) 832.64 Down Time (\$) 425.00 Cascade (\$) 1,000.00 Liners (\$) 4,000.00 Total Cost (\$) 5,425.00 Payback Time NPV @15% r -5,425.00 - -1,080.82 4,344.18 88.2% 2,696.73 3,777.55 88.2% 5,981.56 3,284.83 88.2% 8,837.93 2,856.37 88.2% 11,321.73 2,483.80 88.2% per year \$11,321.73 88.2%

0.00

	Payback Time
years	1.27
months	15.27

15.27



Table V-13,	Economic Analysis for adding Tank 15 to Cascade 2:
A 15%	6 rate of return and 50% tax rate were assumed.

с.

	nours down	\$85.00		
Savings (\$/year)	Savings (\$/month)	Down Time (\$)	Cascade (\$)	Meter (\$)
1,045.01	153.75).00	500.00	0.00
Casn Flow/year		Liners (\$)	íotal Cost (\$)	
\$922.51		0.00	500.00	•
Year	гаураск Тіте	NPV @15%	r i	DCFRR
Û	-500.00	1	·	
1	302.18	802.18	183.5%	325.41
2	999.73	697.55	183.5%	114.78
3	1,60€.30	606.57	183.5%	40.49
4	2,132.75	527.45	183.5%	. 14.28
<u>.</u> 3	2,592.40	458.65	183.5%	5.04
	Der vear	\$2 592 4		\$0.00

Payback Time years 0.61 months 7.27

0.00



Table V-14, Economic Analysis for a Conductivity Meter Without Down-Time Savings:A 50 % tax rate and 15% rate of return was assumed for calcualtions.

Number of Tanks	hours down	price/hour down		
0	13.5	\$85.00		
Savings (\$/year)	Down Time (\$)	Total Savings (\$/year)	Savings (\$/month)]
879.11	0.00	879.11	73.26	
Cash Flow/year	ז ו	Motor (\$)	Total Cost (\$)	1
\$439.56		500.00	500.00	
Vear	Dayback Time	NDV @459		
Ical	Fayback Time	NFV (2015%)	F	DCFRR
^				
0	-500.00			
0	-500.00 -117.77	382.23	83.7%	239.27
0 1 2	-500.00 -117.77 214.60	382.23 332.37	83.7% 83.7%	239.27 130.24
0 1 2 3	-500.00 -117.77 214.60 503.61	382.23 332.37 289.02	83.7% 83.7% 83.7%	239.27 130.24 70.89
0 1 2 3 4	-500.00 -117.77 214.60 503.61 754.93	382.23 332.37 289.02 251.32	83.7% 83.7% 83.7% 83.7%	239.27 130.24 70.89 38.59
0 1 2 3 4 5	-500.00 -117.77 214.60 503.61 754.93 973.47	382.23 332.37 289.02 251.32 218.54	83.7% 83.7% 83.7% 83.7% 83.7% 83.7%	239.27 130.24 70.89 38.59 21.01

Payback Time years 1.34 months 16.07

0.00

Payback Period for the Conductivity Meter \$1,000.00 \$800.00 \$600.00 \$400.00 0 > _{\$200.00} z \$0.00 0.5 1.5 2 2.5 3.5 3 4 4.5 1 -\$200.00 -\$400.00 -\$600.00 Years

	A 50% lax rale	and 15% rate of return	was assumed.	
Number of Tanks	hours down	price/hour down		
8	13.5	\$85.00		
Savings (\$/year)	Down Time (\$)	Total Savings (\$/year)	Savings (\$/monti)]
879.11	9,180.00	10.059.11	838.26	_
Cash Flow/year		Meter (\$)	Total Cost (\$)	
\$5,029.56	1	500.00	500.00	1
Year	Pavback Time	NPV@15%	r	DCFRR
0	-500.00			1
1	3,873.53	4.373.53	1005 9%	45479
2	7,676.60	3.803.07	1005 9%	1 41,12
3	10.983.62	3.307.02	1005 9%	3.72
4	13.859.28	2.875.67	1005 9%	0,34
5	16,359.87	2,500.58	1005,9%	0.03
	per year	\$16,359.87		\$0.00

Table V-15, Economic Analysis for a Conductivity Meter with Down-Time Savings Included: A 50% tax r te and 15% rate £ -----

Payback Time years 0.11 months

(-

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0.00

1.29



f. Water Levels for Cascaded Tanks

A sample calculation is shown for the calculation of tank water level and table V-16 summarizes the results for each set of connections.

Table V-16, Water Level Differences for Each Set of Connections: The desired water level difference for between the two tanks is summarized. This water level difference is necessary for constant overflow.

Connection	Water Level Difference (inches)
15 to 12	1.2
12 to 11	1.0
11 to 8	1.2
4 to 2	0.64

Sample Calculation of Tank Water Level



Need Repolds number.

$$(Z_2 - Z_1) = -2F/q$$

A xibnəqqA

$$\sum_{i=1}^{N} \sum_{i=1}^{N} \sum_{i$$

-

$$\frac{Z}{ZE} = \left(K^{c} + K^{ox} + K^{t} + \frac{\nabla}{1+C}\right)^{\frac{2}{N_{z}}}$$

$$\frac{S}{K^{2}} = \frac{S}{K^{2}} = \frac{S}{K^{2}} + \frac{S}{K^{2}} +$$

 $\frac{z}{2} = \frac{1}{2} \frac{z}{2} \frac{z}{1} \frac{$ 7

2. Automatic Division

a. Original Operating Costs and Water Usage

The original operation costs were calculated similar to the costs of the Metal Finishing Line in section 1-a. Although, chemical costs were not included for the washer systems and the total hours of operation was assumed to be 6,700 annually. Table V-17 shows the results for the Carousel Washer System and table V-18 shows the results for the Crest Washer Systems.

		Water (gal/yr)		Price Data (\$	(cal)		
Tank	Flow (gal/hr)	Generation	Usage	Disposal	Disposal	Water	Sewer	DI System
1		10,868	10,868	sewer	0.00	0.001	0.0020	0,0000
2	150					E Discri		
3		10,868	10,868	sewer	0.00	0.001	0.0020	0.0000
			(10):000 (010072	2008	12 3 9 2 3	
5	i de la constance de la constan La constance de la constance de	10.868			6.2.3919.202.001	e an	0/03/0	1
<u> </u>					600	Stafe al-	S S S 22.9	0(0000
<u> </u>	44.4	00363	5	ACCESSION //	0100		(9)(9)(9)(9)	0.00000
8		2,508	2,160	RCRA	2.06	0.001	0.0020	0.0000
8		0	0	SEWER	<u>e or</u>	6(66)	10 (1 0 ric)	(6)(90)(9)
10	153			Sewer		(3)(-3)	5 (0.37,8)	0.0000
19	60			Seven	000	0.001	0,699.0	0.0027
î î s	Totai ` gailons/day	3,256,020 9,303	3,255,672	· · · ·				

Table V-17, Current Operating Costs for the Carousel Washer System:

gallons/day

34

SAC Units/day

Annual Costs(\$/yr)						heated
Tank	Disposal	Water	Sewer	DI System	Total	tanks
1	0.00	10.87	21.74	0.00	\$32.60	
2	0.00	1.015.87	2,031.74	6(60)		
3	0.00	10.87	21.74	0.00	\$32.60	
4	0.00	10.87	91418	(3)(6)(3)	1925(929)	x
5	0.00	457.03	21.74	0.00	S. 27.3 (27.3)	Y
6	0.00	10,37	61570	0.000	1673/8516	^
7	0.00	62.16.5	(a)	01000	50. C. S. S.	
8	5,166.48	2.16	5.02	0.00	\$5.173.66	
9	0.00	C CC	010.0	0.00		
10	0.00	1.015.37	2:059 7/4	200	6.S. 5 7.253 3	x
- 11	0,00	412.87	8725,74	1,114.74	1. 7. 16 - 76 - 6 - 7 - 1	X

	Disposal	Water Sewer DI System	Total
All Tanks	\$5,166.48	\$3,255.67 \$6,490.30 \$1.114.74	\$16.027.20
Rinse Tanks	\$0.00	\$3,231.78 \$6,441.82 \$1,114.74	\$10,788.34
	0.0%	99.3% 99.3% 100.0%	67.3%

			Water (gal/yr)		Price Data (\$	igal)		
	Tank	Flow (gal/hr)	Generation	Usage	Disposal	Disposal	Water	Sewer	Di System
σ	1		17,500	17,500	sewer	0.00	0.001	0.0020	0.0027
	2	17	113,900	113,900	sewer	0.00	0.001	0.0020	0.0027
)	3	34.5	248,650	248,650	sewer	0.00	0.001	0.0020	0.0027
	4	17	113,900	113,900	sewer	0.00	0.001	0.0020	0.0027
N	1		33,600	33,600	sewer	0.00	0.001	0.0020	0.0027
1	2 0		33,600	33,600	sewer	0.00	0.001	0.0020	0.0027
	3	17	113,900	113,900	sewer	0.00	0.001	0.0000	0,0027
1	4	34.5	264,750	264,750	sewer	0.00	0.001	0.0020	0.0027
J	5	34.5	233,454	233,454	sewer	0.00	0.001	0.0020	0.0027
	6	17	113,900	113,900	sewer	0.00	0.001	0.0020	0.0027
	5 <u>1</u>	Total	1.287.154	1.287.154			1		

 Table V-18, Current Operating Costs for the Crest Washer Systems:

 Waste water generation and annual costs is included.

		Annual Costs(\$iyr)	,		
. T	Tank	Disposal	Water	Sewer	DI System	Total
0	1	0.00	17.50	35.00	47.25	\$99.75
0	2	0.00	113.90	227.80	307.53	\$649.23
0	3	0.00	248.65	497.30	671.36	\$1,417.31
Ø	4	0.00	113.90	227.80	307.53	\$649.23
N	1	0.00	33.60	67.20	90.72	\$191.52
N	2	0.00	33.60	67.20	90.72	\$191.52
N .	3	0.00	113.90	0.00	307.53	\$421.43
N	4	0.00	264.75	529.50	714.83	\$1,509.08
N	5	0.00	233.45	466.91	630.33	\$1,330.69
N	6	0.00	113.90	227 80	307 53	\$649.23

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÷			
	Disposal	Water Sewer DI System	Total
[\$0.00	\$1,287.15 \$2,346.51 \$3,475.32	\$7,108.98
[\$0.00	\$1,202,45 \$2,177.11 \$3,246.63	\$6,626.19
	0.0%	93,4% 92,8% 93,4%	93.2%

b. Annual Savings and Water Reduction

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Annual savings for cascading and spray rinsing were calculated in the same way as in section 1-b. The annual savings for the options for the Carousel Washer System are shown in table V-19 and table V-20. Table V-21 and Table V-22 show the annual savings for the options for the Carousel Washer Systems.

		Water (gal/yr	-		Price Data (1	i/gal)		
Tank	Flow (gal/hr)	Generation	Usage	Disposal	Disposal	Water	Sewer	DI System
-1		10,868	10,868	Sewer	0.00	0.001	0.0020	0.0000
N	150	1,015,868	1,015,868	sewer	00:00	100:0	0.0020	0,0000
ω		10,868	10,868	sewer	0.00	0.001	0.0020	0.0000
4		457,088	10,868	Sewer	0.00	1000	0:0020	00000
GI		10,868	10,868	sewer	0,00	1000	0.0020	0,000
6)		10,868	10,868	sewer	0.00	10000	0.0020	00000
7	66,6	10,868	457,088	sewer	0.00	0.001	0.0000	0.0000
8		2,508	2,160	RCRA	2.06	0.001	0.0020	0.0000
G		0	0	Sewel	0.00	0.001	0.0020	0.0000
10	150	1,015,868	1,015,868	Sewer	0.00	0.001	0.0020	0.0000
11	60	412,868	412,868	sewer	0.00	0:001	0.0020	0.0027
	Total	2,958,540	2,958,192			-		
	Original	3,256,020	3,255,672					

Table V-19, Cascade in the Carousel Washer System: Annual Savings are shown for the rinse tanks alone and for all of the tanks.

Savings gallons/day SAC units/day 297,480 850 3 297,480

×	\$2,353,35	1,114.74	825.74	412.87	0.00	11
×	\$3;047.60	0.00	2,031.74	1,015.87	0.00	10
	\$0.00	0,00	0.00	0.00	00,00	9
	\$5,173.66	0.00	5.02	2.16	5,166.48	8
	\$457.09	0,00	0.00	457,09	0.00	7
	\$32.60	0.00	21.74	10.87	0.00	6
×	\$32.60	0.00	21.74	10.87	0.00	5
×	\$925.04	0.00	914.18	10.87	0.00	4
	\$32.60	0.00	21.74	10.87	0.00	ω
	\$3,047.60	0.00	2,031.74	1,015.87	000	2
	\$32.60	0.00	21.74	10.87	0.00	1
tanks	Total	DI System	Sewer	Water	Disposal	Tank
heated				Yr)	Annual Costs(\$)	

New Costs

 $\left(\right)$

			r
0.0%	\$0.00	\$5,166.48	Disposal
%0.001 %2 <i>6</i> 6 %2	\$2,934,30 \$5,846,86 \$1,114,74	\$2,958 19 \$5,895 34 \$1,114 74	Water Sewer DI System
65.4%	\$9,895.90	\$15,134.76	Total

Original Costs

0.0%	\$0.00	\$5,166.48	Disposal
99.3% 99.3% 100.0%	\$3,231.78 \$6,441.82 \$1,114.74	\$3,255.67 \$6,490.30 \$1,114.74	Water Sewer DI System
67.3%	\$10,788.34	\$16,027.20	Total

Savings

\$0.00	\$0.00	Disposal
\$297.48 \$594.96 \$0,00	\$297 48 \$594 96 \$0.00	Water Sewer DI System
\$892.44	\$892.44	Total

Table V-20:	Spray-Rinsing in the Carousel Washer:	
Values are shown f	or all of the tanks and for the rinse tanks alo	ne

		Water (gal/yr)			Price Data (\$	igal)		
Tank	Flow (gai/hr)	Generation	Usage	Disposal	Disposal	Water	Sewer	DI System
1		10,868	10,868	sewer	0.00	0.001	0.0020	0.0000
2	0	10,868	10,868	sewer	0.00	0.001	0.0020	0.0000
3		10,868	10,868	sewer	0.00	0.001	0.0020	0.0000
4		308,348	10,868	Sewer	0.00	0.001	0.0020	0.0000
5	44.4	10,868	308,348	sewer	0.00	0.001	0.0020	0.0000
6		457,088	10,868	sewer	0.00	0.001	0.0020	0.0000
. 7	66.6	10,868	457,088	sewer	0.00	0.001	0.0000	0.0000
8		2,508	2,160	RCRA	2.06	0.001	0.0020	0.0000
9		0	0	sewer	0.00	0.001	0.0020	0.0000
10	150	1,015,868	1,015,868	sewer	0.00	0.001	0.0020	0.0000
11	60	412,868	412,868	sewer	0.00	0.001	0.0020	0.0027
	Total	2 251 020	2 250 672					

iotai	2,251,020	2,250,672
Original	3,256,020	3,255,672
Savings	1,005,000	1,005,000
gallons/day	2,871	
SAC units/day	10	

	Annual Costs(\$/yr)					heated
Tank	Disposal	Water	Sewer	DI System	Total	tanks
1	0.00	10.87	21.74	0.00	\$32.60	
2	0.00	10.87	21.74	0.00	\$32.60	
3	0.00	10.87	21.74	0.00	\$32.60	
4	00,00	10.87	616.70	0.00	\$627.56	x
5	00.00	308,35	21.74	0.00	\$330.08	x
6	0.00	10.87	914.18	0.00	\$925.04	
7	0.00	457.09	0.00	0.00	\$457.09	
8	5,166.48	2.16	5.02	0.00	\$5,173.66	
9	0.00	0.00	0.00	0.00	\$0.00	
10	0.00	1,015.87	2.031.74	0.00	\$3,047.60	
11	0.00	412.87	825.74	1,114.74	\$2,353,35	X

New Costs

)

Disposal	Water Sewer DI System	Total
\$5,166.48	\$2,250.67 \$4,480.30 \$1,114.74	\$13,012.20
\$0.00	\$2,226,78 \$4,431,82 \$1,114,74	\$7,773.34
0.0%	98.9% 98.9% 100.0%	59.7%

Original Costs

Disposal	Water Sewer DI System	Total
\$5,166.48	\$3,255.67 \$6,490.30 \$1,114.74	\$16,027.20
\$0.00	\$3,231.78 \$6,441.82 \$1,114.74	\$10,788.34
0.0%	99.3% 99.3% 100.0%	67.3%

Savings

Disposal	Water Sewer DI System	Total
\$0.00	\$1,005.00 \$2,010.00 \$0.00	\$3,015.00
\$0.00	\$1,005.00 \$2,010.00 \$0.00	\$3,015.00

			Minéne Imalhar			7-1 7-4- 14			
			valei (yanyi			Price Data (>	rgai)		
	Tank	Flow (gal/hr)	Generation	Usage	Disposal	Disposal	Water	Sewer	DI System
0	-		17,500	17,500	sewer	0.00	0.001	0.0020	0.0027
<u>0</u>	N	0	248,660	0	sewer	000	0.001	00020	0.0027
0	3	345	17,500	248,650	sewer	0.00	0.001	00020	0:0027
0	4	17	006/211	006/01	Sewer	0 8 0	0.001	0,0020	0.0027
z			33,600	33,600	sewer	0.00	0.001	0.0020	0.0027
z	2		33,600	33,600	sewer	0.00	0.001	0.0020	0.0027
N	3	0	233,454	0	sewer	000	1000	0,0000	0.0027
	4		33,600	33,600	sewer	000	1000	0,0020	0.0027
N	07	345	33,600	233,454	sewer	000	0,001	0.0020	0.0027
Ŋ	6	17	006(61)	006/01	Sewer	0.00	1000	0,0020	0.0027
		Total	879,304	828,204					
		Original	1,756,154	1,756,154					
			070 070						

Values are shown for the rinse tanks alone and for all of the tar	Table V-21, Crest Washer Systems Cascade Options:
tanks.	•

927,950

Savings gallons/day SAC units/day 876,850 2,505 9

N	N	z	z	0	0	Ó	0		
6 5 5	3	N	1	4	3	2	1	Tank	
000 000	000	0.00	0.00	0.00	0.00	0.00	0.00	Disposal	Annual Costs(\$/
233.45 113-90	000	ය.හ	33.60	113.90	248,65	0.00	17.50	Water	(yr)
67.20 67.20 227.80	000	67.20	67.20	227,80	35,00	49730	35.00	Sewer	
9072 90733 30753	0,00	90.72	90.72	30753	671.36	0,00	47.25	DI System	
\$191.52 \$930.96 \$649.23	\$0.00	\$191.52	\$191.52	\$649.23	10.5568	06.26t\$	\$99.75	Total	

New Costs

0.0%	\$0.00	\$0.00	Disposal
<u> </u>	\$743:50 \$1,122:30 \$2,007:46	\$828.20 \$1,291.70 \$2,236.15	Water Sewer DI System
88.9%	\$3,873.26	\$4,356.05	Total

Original Costs

		· · ·	_
0.0%	\$0.00	\$0.00	Disposal
93.4% 92.8% 93.4%	\$1,202.45 \$2,177.11 \$3,246.63	\$1,287.15 \$2,346.51 \$3,475.32	Water Sewer DI System
93.2%	\$6,626.19	\$7,108.98	Total

Savings

Disposal \$0.00 00 00 \$458.95 \$1,054.81 -239.17 ß 752.93 ജ

()

	N		Ng		z	Z	0	0	0	0		
	6	5	4	. 3	2	-	4	3	2		Tank	
Total	17	345		0			17	34.5	0		Flow (gal/hr)	
879,304	113,900	33,000	33,600	233,454	33,600	33,600	113,900	17,500	248,650	17,500	Generation	Water (gal/yr
828,204	113,900	233,454	33,600	0	33,600	33,600	113,900	248,650	0	17,500	Usage)
	sewer	sewer	sewer	sewer	sewer	sewer	Sewer	sewer	Sewer	sewer	Disposal	
	000	000	0.00	000	0.00	0.00	0.00	000	0.00	0.00	Disposal	Price Data (\$
	0.001	1000	1000	1000	0.001	0.001	0:001	1000	1000	0.001	Water	/gal)
	0.0020	0,0020	0:0020	0.0000	0.0020	0.0020	0,0020	0.0020	0.0020	0.0020	Sewer	
	0.0027	0.0027	0,0027	0.0027	0.0027	0.0027	0.0027	72000	0.0027	0.0027	DI System	

Table V-22, Spray-Rinse Options for the Crest Washer Sytstem: Values for the rinse tanks alone and for all of the tanks are shown.

Original Savings gallons/day SAC units/day 1,756,154 876,850 2,505 9 1,756,154 927,950

Tank
 Annual Costs(\$/yr)

 Disposal
 Water

 0.00
 17.50

 0.00
 248.65

 0.00
 248.65

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60

 0.00
 33.60
 Sewer 35,00 497,30 35,00 227,30 67,20 67,20 67,20 67,20 DI System 47.25 0.00 671.36 307.53 90.72 90.72 90.72 90.72 90.72 90.72 30.733 \$000 \$191.52 \$191.52 \$191.52 \$191.52 \$191.52 \$191.52 \$191.52 \$191.52 \$191.52

Total

ZZZZZZOOOO

	New
1	Costs

തിഗ്ദ

000

90

(8)0

0.0%	\$0.00	\$0.00	Disposal	
% 8.68 %6.98 %8.68	\$743:50 \$1,122:30 \$2,007:46	\$828.20 \$1,291.70 \$2,236.15	Water Sewer DI System	
88.9%	\$3,873.26	\$4,356.05	Total	

Origin

8	8	Dis	ial Costs
8	. <u>8</u>	oosal	
\$1,202.4	\$1,287.1	Water	
5 \$2,17	5 \$2,340	Sew	
7.11 \$3,	551 \$3.	rer Di S	
246.63	47532	System	1
\$6,626.19	\$7,108.98	Total	
	\$0.00 \$1.202.45 \$2,177.11 \$3:246.63 \$6,626.19	\$0.00 \$1,287,15 \$2,346,51 \$3,475,32 \$7,108,96 \$0.00 \$1,202,45 \$2,177,11 \$3,246,63 \$6,626,19	Disposal Water Sewer Di System Total \$0.00 \$1,287,15 \$2,346,51 \$3,475,32 \$7,108,96 \$0.00 \$1,202,45 \$2,177,11 \$3,246,63 \$6,626,19

Savings

Disposal \$0.00 \$0.00 \$458.95 | \$1,054.81 \$458.95 | \$1,054.81 Water D System \$2,752.93 \$2,752.93 Total

c. RO Reject Potential

The calculation for the potential annual savings from the use of RO reject water for the Carousel Washer System is shown below. Table V-34 in appendix B, section 2-b shows the average daily RO reject volume of 2,678 gallons, which was used for the following calculations.

$$\begin{pmatrix} 2,16 \frac{18 \text{ qal}}{\text{day}} \\ \frac{350 \text{ day}}{\text{yar}} \end{pmatrix} = 937,300 \text{ qal}/\text{yar}$$

Notar =7 \$0.001/qal

seven =7 \$0.0025/qal.

$$\begin{pmatrix} 937,300 \text{ qal} \\ \text{yar} \end{pmatrix} \begin{pmatrix} $0.001 + $0.0025.] \text{H} \\ \text{qal} \end{pmatrix}$$

$$\begin{pmatrix} = $3,280.55 \\ \text{Annual Savings} \end{pmatrix}$$

d. Economic Analysis

Economic calculations were performed in the same manner as in section 1-d. Table V-23 and table V-24 show the economic analysis for the Carousel Washer System. Table V-25 and table V-26 show the economic calculations for the Crest Washer Systems. Finally, table V-27 shows the economics of using the RO reject water for the Carousel Washer System.

Table	V-23, Economic	Analysis for (Carousel Wasi	her System	Cascde Option:
	A 50% tax	rate and 15%	s rate of return	n was assun	ned.

Annual Savings		SAC Savings	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		
Carousei (\$/yeart)	Crest (\$/year)	Carousel (\$)	Crest (\$)	DI (\$)		
892.44	0.00	2,850.00	0.00	0.00		
Annual	SAC		Cash Flow/year	Cash Flow Year 1		
Savings (\$/year)	Savings (\$)		\$446.22	\$1,871.22		
892.44	2,850.00]				
Conto						
	Spray (\$)	DI (\$)	Other (f)	Total Cost (\$)		
				1 000 00		
1,000.00	0.00	0.00	0.00	1,000.00		
Year	Payback Time	NPV @15%	r	DCFRR		
0	-1,000.00					
1	627.15	1,627.15	122.2%	842.32		
2	964.55	337.41	122.2%	90.42		
3	1,257.95	293.40	122.2%	40.70		
4	1,513.08	255.13	122.2%	18.32		
5	1.734.93	221.85	122.2%	8 25		
	Der vear	1.734.93	<u> ''''''''''''''''''''''''''''''''''''</u>	\$0.00		
years months	0.75 9.01	0.00				
\$2,000.00	Payback Tim	e for Carousel Ca	scde			
\$1,500.00 -						
\$1,000.00		<u>_</u>				
> \$500.00 - L	•					
\$0.00	1 1.5	2 2.5 3	3 3.5 4	4.5 5		
-\$500.00						
-\$1,000.00	· · · · · · · · · · · · · · · · · · ·					
		Years				

Annual Savings		SAC Savings		- <i>i i</i> i i
J 317 56		Carousel (\$)	Crest (\$)	DI (\$)
1,317.30	0.00	0.00	0,000.00	0.00
Annual	SAC	٦	Cash Flow/vear	Cash Flow Year 1
Savings (\$/year)	Savings (\$)		\$658.78	\$3,983,78
1,317.56	6,650.00			1
Casta				
Costs	Specie (\$)	DL (#)	Other (f)	Total Cost (f)
1 000 00	3pray (3)			1 000 00
1,000.00	0.00	1 0.00	0.00	1,000.00
Year	Payback Time	NPV @15%	r	DCFRR
0	-1,000.00			
1	2,464.16	3,464.16	319.0%	950.86
2	2,962.29	498.13	319.0%	37.53
3	3,395.45	433.16	319.0%	8.96
4	3,772.11	376.66	319.0%	2.14
5	4,099.64	327.53	319.0%	0.51
	per year	r 4,099.64		\$0.00
5	Pavback Time			
•		0.00		
Veare	0.21			
years months	2.57 Payback Time fo	or Cascade Tank N	5 and N4	
years months \$5,000.00	2.57 Payback Time fo in the Cr	or Cascade Tank N rest Washer System	5 and N4 1	
years months \$5,000.00	2.57 Payback Time fo in the Cr	or Cascade Tank N rest Washer System	5 and N4 1	
\$5,000.00	2.57 Payback Time fo in the Cr	or Cascade Tank N est Washer System	5 and N4 1	
\$5,000.00 \$4,000.00	2.57 Payback Time fo in the Cr	or Cascade Tank Na est Washer System	5 and N4	
years months \$5,000.00 \$4,000.00	2.57 Payback Time fo in the Cr	or Cascade Tank N rest Washer System	5 and N4	
\$5,000.00 \$4,000.00 \$3,000.00	2.57 Payback Time fo in the Cr	or Cascade Tank N	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00	0.21 2.57 Payback Time fo in the Cr	or Cascade Tank Na rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00	0.21 2.57 Payback Time fo in the Cr	or Cascade Tank Na rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$3,000.00	0.21 2.57 Payback Time for in the Cr	or Cascade Tank Na rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00	0.21 2.57 Payback Time fo in the Cr	or Cascade Tank Na rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00 2 2	0.21 2.57 Payback Time fo in the Cr	or Cascade Tank N rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00 2 \$2,000.00	0.21 2.57 Payback Time for in the Cr	or Cascade Tank Ni rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00 \$2,000.00 \$2,000.00 \$2,000.00	0.21 2.57 Payback Time for in the Cr	or Cascade Tank N	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,2000.00 \$2,1,000.00 \$1,000.00	0.21 2.57 Payback Time for in the Cr	or Cascade Tank Na rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00 2 \$1,000.00	Payback Time for in the Cr	or Cascade Tank Na rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00 \$2,000.00 \$1,000.00 \$0.00	0.21 2.57 Payback Time for in the Cr	or Cascade Tank Na rest Washer System	5 and N4	
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00 \$1,000.00 \$0.00 \$0.00 \$0.5	0.21 2.57 Payback Time for in the Cr	or Cascade Tank Na rest Washer System	5 and N4	4.5 \$
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2 \$2,000.00 \$1,000.00 \$0.00 \$0.00 \$0.5	2.57 Payback Time for in the Cr	2 2.5 3	5 and N4	4.5 5
years months \$5,000.00 \$4,000.00 \$3,000.00 \$3,000.00 \$2,000.00 \$1,000.00 \$0.00 \$0.5 \$1,000.00	0.21 2.57 Payback Time for in the Cr	or Cascade Tank Na rest Washer System	5 and N4	4.5

 Table V-25, Economic Analysis for the Cascade Options for the Crest Systems:

 A 50% tax rate and a 15% rate of return was assumed.

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Table V-26,	Economic Analysis for the Cascade Options for the Crest Washer Systems:
	A 50% tax rate and a 15% rate of return was assumed.

Annual Savings	· · · · · · · · · · · · · · · · · · ·	SAC Savings		
Carousel (\$/yeart)	Crest (\$/year)	Carousel (\$)	Crest (\$)	RO (\$)
2,752.93	0.00	0.00	8,550.00	0.00
Annual	SAC	7	Cash Flow/year	Cash Flow Year 1
Savings (\$/year) 2,752.93	Savings (\$) 8,550.00		\$1,376.47	\$5,651.47
Costs				
Cascade(\$)	Spray (\$)	RO (\$)	Other (\$)	Total Cost (\$)
0.00	1,000.00	0.00	0.00	1,000.00
- 41°				
Year	Payback Time	NPV @15%	r	DCFRR
0	-1,000.00			<u> </u>
1	3,914.32	4,914.32	493.0%	952.96
2	4,955.13	1,040.81	493.0%	39.14
3	5,860.18	905.05	493.0%	6.60
4	6,647.18	787.00	493.0%	1.11
5	7,331.53	684.35	493.0%	0.19
	per year	7,331.53		\$0.00

Payback Time 0.10 years months 1.16

0.00





Appendix A

Annual Savings	ı	SAC Savings		
arousel (\$/yeart)	Crest (\$/year)	Carousel (\$)	Crest (\$)	RO (\$)
3,280.55	0.00	0.00	0.00	8,550.00
Annual	SAC	1	Cash Elowhear	Cash Flow Voor
Savings (S/vear)	Savings (\$)		\$1 RAD 2R	\$5 915 28
3,280.55	8,550.00		L	40,710.20
Costs				
Cascade(\$)	Spray (\$)	RO(\$)	Other (\$)	Total Cost (\$)
0.00	0.00	1,500.00	0.00	1,500.00
Year	Payback Time	NPV @15%		DCEPP
0	-1.500.00			DUFRK
1	3.643.72	5,143,72	327.6%	1 383 27
2	4,884.00	1,240.29	327.6%	89 70
3	5,962.52	1,078.51	327.6%	20.98
4	6,900.35	937.84	327.6%	4.91
5	7,715.86	815.51	327.6%	1.15
	per year	1,640.28		\$0.00
months	2.77			
months	2.77 Payback Time for Re	O Reject Tank and	l Plumbing	
months \$8,000.00	2.77 Payback Time for R	O Reject Tank and	l Plumbing	·····
\$8,000.00 \$7,000.00	2.77 Payback Time for R	O Reject Tank and	d Plumbing	•
months \$8,000.00 \$7,000.00 \$6,000.00	2.77 Payback Time for R	0 Reject Tank and	1 Plumbing	•
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00	2.77 Payback Time for R	O Reject Tank and	4 Plumbing	
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00 \$4,000.00	2.77 Payback Time for R	O Reject Tank and	d Plumbing	
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00 \$4,000.00 \$3,000.00	2.77 Payback Time for R	O Reject Tank and	d Plumbing	
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00 \$4,000.00 \$3,000.00 \$2,000.00	2.77 Payback Time for R	O Reject Tank and	4 Plumbing	
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00 \$3,000.00 \$2,2,000.00 \$1,000.00	2.77 Payback Time for R	O Reject Tank and	4 Plumbing	
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00 \$4,000.00 \$3,000.00 \$1,000.00 \$0.00	2.77 Payback Time for R	O Reject Tank and	4 Plumbing	
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00 \$4,000.00 \$3,000.00 \$2,000.00 \$1,000.00 \$0.00 \$0.00 \$0.5	2.77 Payback Time for Re	O Reject Tank and	4 Plumbing •	4.5
months \$8,000.00 \$7,000.00 \$6,000.00 \$5,000.00 \$5,000.00 \$3,000.00 \$2,000.00 \$1,000.00 \$0.00 \$0.00 \$2,000.00 \$0.00 \$0.00 \$2,000.00	2.77 Payback Time for Re	O Reject Tank and	4 Plumbing • •	4.5

Table V-27, Economic Analysis of RO Reject Option: A 15 % rate of return and 505 tax rate was assumed.

B. TEST RESULTS

1. Machining Division and Kurt Gear Division

a. Conductivity Data

*	<i>Γable V-28, Conductivity Readings Measured in μS/cm:</i>	
Events are	noted by the given date. Readings were taken throughout the do	u

		Tank	3	5	6	8	11	12	15	16	well	RO	city (c)	city (h)
	6/27/97	2:45	75	519	141	1161	5720	16	85	9		1		
M	6/30/97	3:00	83	571	14	996	1311	36	1	2		1		
		4:15	74	555	12	985	1411	39	1	1		1		×
	7/1/97	3:25	77	391	20	1595	1030	43	8	3		7		
	7/2/97	10:15	59	222	5	818	2400	17	58	3	601	1		
		10:50	51	206	6	905	1847	22	53	3	643	0		
		1:15	53	181	5	767	1730	30	47	4	587	0		
	tanks	2:15	54	210	13	831	1685	24	55	3	635	0		
	cleaned													<u> </u>
	7/3/97	10:30	0	0	0	0	527	0	0	0	506	0		
M	7/7/97	10:00	0	0	0	0	516	0	0	0	513	0	388	418
		1:15	18	162	0	115	813	6	0	10	546	0	297	430
-		3:30	55	353	7	218	1545	16	0	21	450	0	286	361
	7/8/97	10:30	61	200	5	303	1302	11	45	10	289	0	132	284
		11:30	39	188	4	351	1138	11	29	21	459	0	281	477
		1:30	59	210	3	389	1872	16	47	19				
	1 <u>1</u> .	2:20	75	259	3	426	1599	13	50	20				
	7/9/97	8:45	112	237	3	525	2030	7	109	19	509	0		
	cascade	1:15	101	135	2	508	1404	12	120	12	578	0		
	15,16													
	7/10/97	10:15	61	105	0	260	598	4	7	4	305	0		
		11:15	87	104	3	597	663	5	122	7	515	0		
		12:45	96	105	5	641	236	3	71	2	316	0		
		1:15	70	60	0	317	312	1	84	2	360	0		
	7/11/97	10:00	61	129	2	526	717	5	78	2	561	0		
		11:00	93	155	3	716	1155	5	111	1	575	0		
		12:00	98	142	2	678	890	5	121	4				
, [2:00	98	109	0	578	761	7	109	3	499	0		
×.	7/14/97	10:15	103	75	2	605	754	0	0	0	760	0		
[slow flows	10:45	116	36	5	631	630	2	30	0	552	0		
		1:15	161	64	2	619	680	5	97	2	52	0		
		4:00	87	72	2	732	585	3	82	2	556	0		
[7/15/97	9:00	70	32	5	163	261	_7	20	7	161	0		
		12:00	58	275	5	92	97	2	14	1				
	7/16/97	9:15	82	539	10	324	2480	12	29	4				
ľ		11:30	103	265	6	81	1400	9	8	4	226	0		
ľ		1:00	138	306	6	61	1600	11	7	4				
F	7/18/97	3:30	94	180	5	630	758	8	93	3				
WT	7/23/97	11:15	89	94	2	125	738	9	30	5				
ſ		12:00	39	133	3	182	1345	14	51	9				
Ī	-	2:00	192	374	6	740	1435	17	88	30				

Table V-28 shows all conductivity readings of the rinse water. Fresh water flow-rates were decreased on July 14. The conductivity of the rinse water did not change significantly with the reduced fresh water flow-rates. This suggest that the virgin rinse water is being drained. Tank 11 is fed with city well water and hence the conductivity readings are significantly greater than the rest of the rinse water.

b. Temperature Data

In general, the RO water has a higher temperature than the city well water. The temperature of the water in Tank 16 and Tank 15 was recorded throughout the days when the two tanks were cascaded. All of the recorded temperature readings are found in table V-29. From these numbers an average temperature change could be determined. From that value the additional cost for heating Tank 16 was calculated.

Table V-29, Temperature Readings:

The temperature difference between the set temperature of 136°F and the actual temperature for tank 16 is recorded. This temperature difference was used to determine the additional electric cost needed for heating the water if constant overflow occurs.

1		Temper	rature (°F)				
Date	Time	well	Tank 11	Tank 15	RO	Tank 16	$\Delta \mathbf{T}$
7/9/97	8:45	62	62	82	72	120	16
	1:15	66	64	100	76	136	0
7/10/97	10:15	66	65	87	75	135	1
	11:15	62	64	87	76	136	0
	12:45	61	64	89	79	123	13
	1:15	63	61	94	75	136	0
7/11/97	10:00	60	62	101	75	119	17
	11:00	59	60	102	75	123	13
7/14/97	10:15	71	71	75	80	123	13
	10:45	69	72	72	78	136	0
	1:15	80	72	85	80	136	0
	4:00	60	60	96	81	136	0
7/15/97	9:00	58	61	102	78	126	10
7/16/97	11:30	65	65	101	79	135	1

c. pH Data

Table V-30, pH Readings:

Events are noted by the given date. Readings were taken throughout the day. In general, the pH of the rinse water in each tank plateaus after a certain point is reached. The rinse water pH does depend on the pH of the fresh water.

2	Tank	3	5	6	8	11	12	15	16	well	RO	city	city
								· .				(cold)	(hot)
6/27/97	2:45	9.19	10.83	8.22	3.03	7.00	5.30	4.01	4.87		5.74		
6/30/97	3:00	9.15	10.93	7.91	3.13	7.00	5.18	6.41	5.71		5.75		
	4:15	9.15	10.91	8.11	3.14	7.00	5.00	6.34	5.54		6.04		
7/1/97	3:25	8.97	10.49	7.83	2.78	7.26	4.78	5.10	5.51		5.39		
7/2/97	10:15	9.01	10.28	7.39	2.96	8.54	5.41	3.97	5.27	7.61	5.08		
	1:15	9.03	10.21	7.39	2.90	8.09	4.63	4.05	5.95	7.49	5.39		
tanks	2:15	8.97	10.32	7.65	2.91	8.11	4.56	4.02	5.99	7.44	5.67		
cleaned													
7/3/97	10:30	6.53	6.33	6.36	8.46	7.62	7.52	5.13	6.23	6.69	5.60		
7/7/97	10:00	8.21	6.17	5.85	6.72	7.42	5.14	4.96	4.99	7.41	5.19	7.28	7.02
	1:15	9.06	10.67	7.41	4.01	7.00	5.56	5.39	4.52	7.57	4.62	7.39	7.00
	3:30	8.95	10.75	7.39	4.01	7.00	4.86	5.19	4.01	7.54	5.43	7.44	7.00
7/8/97	10:30	8.66	10.52	7.96	3.09	6.28	5.28	3.95	3.91	7.50	5.51	7.24	7.03
	11:30	8.97	10.63	8.11	3.07	3.59	4.58	3.89	3.92	7.51	5.73	7.37	7.10
	1:30	9.00	10.75	7.69	2.99	6.53	5.16	3.92	3.91				
	2:20	8.99	10.70	7.44	2.99	6.57	4.78	3.81	3.86				
7/9/97	8:45	9.00	10.66	7.49	3.10	6.72	5.74	3.67	4.10	7.55	5.50		
cascade 15,	1:15	9.00	10.29	7.34	3.01	7.04	5.43	3.62	4.68	5.58	7.55		
16					-								
7/10/97	10:15	8.94	10.03	8.14	2.92	7.27	5.10	3.62	4.54	7.45	5.32		
and and a second se	11:15	8.95	10.06	7.74	2.86	7.59	5.07	3.50	4.12	7.50	4.68		
	12:45	8.79	10.02	7.40	2.84	7.90	4.89	4.38	4.39	7.39	5.64		
	1:15	8.94	9.98	7.03	2.84	7.94	4.76	3.34	4.37	7.48	5.51		
7/11/97	10:00	8.92	10.24	7.42	2.95	7.53	5.27	3.63	4.79	7.49	5.92		
	11:00	8.97	10.24	7.14	2.96	7.59	5.29	3.55	4.96	7.52	5.72		
	12:00	8.96	10.26	7.51	2.94	7.61	5.49	3.91	5.14				
	2:00	8.96	10.02	7.32	2.95	7.76	5.43	3.45	4.80	5.59	7.52		
7/14/97	10:15	9.84	9.60	6.90	2.85	7.81	6.06	5.63	7.54	7.54	5.50		
slow flows	10:45	8.96	9.54	6.56	2.81	7.89	5.56	4.96	5.19	7.03	5.40		
	1:15	8.86	9.61	7.13	2.93	8.03	5.53	3.69	5.18	7.29	5.44		
	4:00	8.96	9.61	7.07	2.85	7.75	5.00	3.68	5.47	7.39	5.05		
7/15/97	9:00	9.05	10.62	7.32	3.08	7.00	5.14	4.13	5.53	7.59	5.15		
	12:00	9.07	10.65	8.18	3.95	7.38	5.20	3.92	5.18				
7/16/97	9:15	9.02	10.69	7.58	3.40	6.10	5.97	4.30	5.48				
	11:30	9.05	10.85	8.03	4.20	4.95	4.93	4.45	4.66	7.62	5.57		
	1:00	9.06	11.01	7.94	3.75	6.44	4.95	4.33	4.37				
7/18/97	3:30	8.90	9.98	6.37	2.96	7.55	4.80	3.29	4.33				
7/23/97	11:15	8.62	10.23	6.55	3.18	6.47	4.25	3.27	4.01				
	12:00	8.64	10.36	6.47	3.27	10.01	4.02	3.56	4.01				
	2:00	8.62	10.36	5.01	3.33	3.94	4.50	4.50	4.01				

Table V-30 shows all pH readings of the rinse water. Fresh water flow-rates were decreased on July 14. After the floe-rates were decreased, the pH of the rinse water did not change significantly with the reduced fresh water flow-rates. This again suggests that the virgin rinse water is being drained. Because Tank 11 is fed with city well water, the pH change is not on the same scale as the other rinse tanks. RO water generally maintains a pH of about 5 and city well water usually has a pH of about 7.

d. pH and Conductivity Measurements when Tanks were Cleaned

Table V-31 summarizes the pH and conductivity measurements for the days when the tanks were cleaned out. These measurements show the variability and inconsistency of rinse tank cleaning.

Table V-31, pH and Conductivity Measurements when Tanks are Cleaned: Readings were taken before the tanks were drained and cleaned. The conductivity is measured in μS/cm. Only some of the tanks are cleaned each week.

Date	7/3/97		7/11/97	· · · · · · · · · · · · · · · · · · ·	7/18/97	· · · · · · · · · · · · · · · · · · ·
Tank	μ S/cm	pH	μ S/cm	pН	μ S/cm	pH
3	54	8.97			94	8.90
5	210	10.32			180	9.98
6	13	7.65			5	6.37
8	831	2.91	678	2.96	630	2.96
11	1685	8.11				
12	24	4.56	5	5.49		
15	55	4.02	121	3.91	93	3.29
16	3	5.99				

e. Tank 11 Profile Data

Specific concern was expressed about the pH of the rinse water in Tank 11. Manual addition of caustic was not done throughout the testing day. Hence the natural course or the rinse water pH and conductivity could be monitored. Table V-32 shows the collected rinse water data.

Conductivity and pri measurements were taken throughout the day.						
Time (min)	pH	Time (mi	in) Conductivity (µS/cm)	comment		
0	6.32	0	776	1		
5	2.73	5	447	after parts rinsed		
10	2.73	10	471			
15	2.75	15	430			
20	8.57	20	902 \	caustic was added		
27	5.91	27	801 \	after parts rinsed		
35	6.01	35	854			
40	6.11	40	692			
50	6.73	50	678			
60	6.32	60	614			
65	6.41	65	683 \	5=69		
75	3.09	75	641	after		
80	3.13	80	539			
85	3.14	85	369			
90	3.15	90	399			
95	2.55	95	471			
100	2.57	100	1667	$\Delta = 1/96$		
105	2.59	105	629			
110	2.61	110	700			
115	2.64	115	702			
120	2.33	120	689	after		
125	2.34	125	795	4=106		
130	2.36	130	508	· · · · · · · · · · · · · · · · · · ·		
140	2.38	140	668			
145	2.19	145	1969	$\Delta = (301)$ after		
150	2.21	150	3180	A=12117 2512		
155	2.23	155	757	4		
160	2.24	160	1085 1			
165	2.24	165	944			
170	2.11	170	1380	after parts rinsed		
175	2.11	175	1064	A=4.36		
180	2.12	180	438			
185	2.13	185	720			
190	2.09	190	7760	after parts rinsed		
195	2.09	195	4580	x=7040		
230	2.04	230	5320			
235	2.03	235	3810			
240	2.03	240	5610			
245	1.99	245	7710	after parts rinsed		
250	2.01	250	7900	x= 4090		
255	2.07	255	7660	· · · · · · · · · · · · · · · · · · ·		
265	2.13	265	6940 🔰			

Table V-32, Tank 11 Rinse Water Measurements:

tap water 211.5gph

Because of the concerns caustic solution is added to the tank manually. One option is to install an pH metering pump control system. Before this could be done, the necessity of such a system needed to be investigated. Figure V-2 shows the pH profile of the rinse water in Tank 11. The pH profile shows how the pH of the water drops quickly until a value of pH 2 is reached.



Figure V-2, Plot of the Rinse Water pH for Tank 11: The peak at 9.5 occurred after caustic solution was added to the tank manually. After parts are rinsed, the pH drops drastically until it reaches a value of about pH 2.

2. Automatic Division

a. Conductivity Measurements

A preliminary assessment of the waste water generation problem at the Automatic Division was conducted on March 19, 1997. Karl DeWahl, MnTAP, collected conductivity and water flow measurements from the Carousel Washer System. The report can be found in appendix D. Table V-33 summarizes the conductivity measurements of the rinse tanks within the Carousel Washer System.

Table V-33, Conductivity Measurements from the Carousel Washer System: All tanks receive city well water as a feed stream except for Tank 11 which receives RO water as a feed.

	Tank	Conductivity (µS/cm)
- 1020 	2	394-396
	4	395-410
and a second	5	395-405
and the second sec	б	394-399
12."	7	360
- 6 32	9	397-404
	10	375-380
	11 -	4

b. Meter Readings

After the original 30-day waste water generation study, specific areas of the plant were monitored for waste water generation. Meter readings indicated that the Carousel Washer System generated most of the waste water as compared all systems. Tank 9 was converted from a dip-rinse to a spray-rinse. In addition, the four tank dip-rinse series— Tank 4, Tank 5, Tank 6, and Tank 7—was converted to two sets of cascaded diprinses—Tank 4 and Tank 5, and tank 6 and Tank 7. After these modifications were made to the Carousel Washer System, an additional 14day study was conducted. Table V-34 shows the meter readings from the 14-day study. In addition, the top portion of the table displays the meter readings which determined the areas of high waste water generation.

	(RO sy	stem Usag	ge) and Was	sher (C	Carousel	Washer S	System Us	sage).
	Date	RO Feed	RO Stored	RO	Reject	Washer	Total	Reading
	20-May					6677		
	21-May	8032	5214	2818	35.1%	9520	17552	
	22-May	7432	4834	2598	35.0%	\ 8470	15902	
F	23-May	5833	3808	2025	34.7%	7016	12849	
T	27-May	14020	9220	4800	34.2%	3144	17164	
	28-May	5239	3438	1801	34.4%	8997	14236	
	29-May	6817	4432	2385	35.0%	9373	16190	
F	30-May	7497	4886	2611	34.8%	9390	16887	
M	2-Jun	15663	10165	5498	35.1%	21197	36860	
	3-Jun	6020	3935	2085	34.6%	14219	20239	
	4-Jun	6280	4105	2175	34.6%	3114	9394	
	5-Jun	6694	4342	2352	35.1%	9170	15864	
F	6-Jun	7510	4885	2625	35.0%	10070	17580	
M	9-Jun	13468	8770	4698	34.9%	15472	28940	
	10-Jun	5183	3349	1834	35.4%	7188	12371	
	11-Jun	7104	4604	2500	35.2%	9303	16407	
- · - [12-Jun	4071	2672	1399	34.4%	3491	7562	
F	13-Jun	2821	1856	965	34.2%	2081	4902	
	14-day	study						
	begi	ns						······
Т	17-Jun	15019	9801	5218	34.7%	29279	44298	50650
	18-Jun	4975	3249	1726	34.7%	2884	7859	11840
	19-Jun	4276	2827	1449	33.9%	1114	5390	9040
F	20-Jun							11980
М	23-Jun							30010
Th	26-Jun							37260
F	27-Jun							19690
M	30-Jun	· · · · ·						21000
	1-Jul						•	32640
	2-Jul							13860
Th	3-Jul							10620
T	8-Jul							34620
	9-Jul							19370
	10-Jul							15630
F	11-Jul							17510
	14-day stu	dy ends		·				
M	14-Jul							22790
	15-Jul							15900
	16-Jul	1						20400

Table V-34, Meter Readings at the Automatic Division: All values are recorded in gallons. The total column is the sum of the RO Feed

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C. PROCESS DRAWINGS

Figure V-3 shows a detailed schematic of the Metal Finishing Line. Piping, heating units, and control valves are shown on the diagram. A drawing of the pH adjustment system is shown in figure V-4. Finally, figure V-5 shows a drawing of the weir construction used for Cascade 1 and suggested for Cascade 2.





To Sewer

Figure V-4: Schematic of the pH Adjustment System for the Metal Finishing Line. Throughout processing waste water enters the tank through the sump line, but when the tanks are cleaned waste water enters the tank through the air pump line. The pH probe inside the tank triggers pumps to add sulfuric acid and caustic when the pH is above 9.5 and below 5.5 respectively. While the pH is being adjusted, the control valve closes to keep the waste water from entering the sewer. Once the pH has reached a valid number the valve opens and waster water is emptied into the sewer. Finally, the second pH probe monitors the pH of the water entering the sewer. An alarm will light up when the waste stream pH is outside of the regulated range (5 to 10).

Appendix C



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(a) Front View



Figure V-5, Diagram of Weir Construction:
(a) The weir itself is located on the outside of the tank. One side is two inches wide and the other is three inches wide. The slope helps push water down the drain. The drain opening in shown.
(b) One inch holes are evenly spaced in a straight line. These holes are in the side of the tank and allow flow into the outside weir.

Appendix D

D. Additional Information

Karl DeWahl from MnTAP visited the Automatic Division in March 1997 to access the facilities waste water generation. Rinse water conductivity measurements and water flow rates were collected for the Carousel Washer System. Water reduction options, which can also improve rinse quality, were suggested. The four suggestions include reusing RQ water, redesign or modify current tank system, check carousel arms for leaks, and clean tank walls. After this initial meeting in March, the Carousel Washer System was modified to include a spray rinse in Tank 9 and two sets of cascaded rinse tanks—Tank 4 and Tank 5, and Tank 6 and Tank 7. The report is attached on the following pages.

April 1; 1997

Jim Sjoselius Kurt Manufacturing Company 5280 Main St Minneapolis, MN 55421

Dear Jim Sjoselius:

On 3/19/97 we collected water flow rates and bath conductivity measurements at the Northdale facility. We did not have a facility water use total to compare, but the sum of the individual flows seems considerably less than I expected to find based on your general comments. Further efforts to identify other water uses or leaks may be necessary. However, the reading taken do suggest a number of possible ways to reduce water usage and probably also to improve rinsing effectiveness. I will summarize the flow and conductivity data we collected and then present the conclusions I draw from the data and what I see as your water reduction alternatives.

The flows we identified were:

	conductivity(us)	estimated gpy	estimated gpm	estimated value
domestic water 20 gpd x # of people	;	not calculated	_ · ·	\$-/ут
carousel washer tank #1 alk cleaner		small	, – · .	-
tank #2 rinse	394-396	480,000	2.0	1536
tank #3 alk cleaner		small		
tank #4 heated rinse	395-410	120,000	0.5	384
tank #5 heated rinse	395-405	120,000	0.5	384
tank #6 rinse	394-399	240,000	-1	768
tank #7 rinse	360	240,000	· 1. T	768
tank #8 desmut		small	· -	· 1.1
tank #9 rinse (cloudy)	397-404	1,440,000	6	4608
tank #10 heated rinse	375-380	600,000	2.5	1920
tank #11 hot DI rinse	4	240,000	1.0	768
crest console tank #1 alk cleaner		small .	-	
tank #2 dead rinse		small	- • •	- 1 C
tank #3 spray rinse on 1905	out of 400	1,032,000*	2.2 .	3302
tank #4 rinse ~ continuous F6	L)	168,000	0.7	537
tank #5 rinse	-	168,000	0.7	537
tank #6 &7 dry		no water use		
vibratory deburring	· ·	unknown	· · ·	
thermal deburring		unknown	· · · · ·	
coolant make-up		unknown		· · ·
	total =	over 4,848,000	. 0	ver \$15,500

Note that the water cost does not reflact the additional cost of providing deionized water.
Observations & Conclusions

1. Incoming city water feeds had a conductivity of about 190ys. Seven of the eight rinse tanks had conductivities around 400ps which did not noticeably change as parts loads were brought into the tanks or taken out. Parts as they were immersed in additional rinses as they went through the first 7 did not come into contact with cleaner water.

Conclusion - Fresh water feeds to each tank is not producing fresh water results. Parts go into "used" water that has twice the ionic contamination of tap water.

2. The DI rinse had a significantly lower conductivity than any other rinse, but this conductivity did not increase as parts were placed in the tank.

Conclusion - The de-ionized water is being under-utilized. It is being sent to drain in nearly virgin condition - it is certainly much cleaner than the tap water being used for most of the rinses.

3. Tanks turn-over their volume in 25 minutes for tank #9 and 300 minutes for tanks #4&5, compared to the time between loads of roughly 5 minute for each tank.

tank size Conclusion - The tanks are too large for efficient rinsing. Contaminants rinse off parts and are dispersed & ×48248" diluted in a large volume of water, and then are only slowly purged from the system. I estimate tank volumes at roughly 150 gallons each, while the space a loaded rack can fit in is about 8 gallons. est indeel rack top view 8"xx 15" x 15'

4. Inlets and outlets are located within inches of each other on tanks 4.& 5.

5. Tank conductivity occasionally spiked when a carousel arm carrying no load entered a tank. Conclusion - The welded tubular, carousel structure may have pin-hole leaks that serve to transport far greater amounts of contaminants from tank to tank than the than parts carry-over does.

6. Conductivity changed slightly with location, The center of the tank had the highest conductivity, while area near the wall had the lowest.

Conclusion - There is very little mixing in the rinse tanks. Contaminants are moved away from surfaces by diffusion - a slow process.

7. There is a small build-up of scale or solids on the walls of most of the tanks. This may be a source of buffering or internal storage of ionic contamination that may serve to make the rinse water dirtier than it needs to be.

Water use reduction options

A. Reuse the DI water. Cascade it back into previous rinses as many times as possible, until its conductivity or other characteristics show it is degraded worse than tap water. Other characteristics that might be important are pH, turbidity, and oil content. We did not measure the conductivity on any rinses in the Crest console wash, but odds are that effluent could be reused on the carousel system also, and could be used in one of three ways:

Replace the present carousel DI feed, cutting overall DI water consumption.

- Add flow (greater tank turn-over and mixing) to cascaded rinses.
- Replace tap water flow on up stream rinses if the DI water from cascading tank #9 water becomes too contaminated to replace all the fresh water feeds.

B. . Redesign or modify the tank system. I realize the carousel washer was not designed for the current product and that there is a value in retaining capacity for future flexibility.

Reduce the effective size of the tanks to improve turn-over, mixing and the purging of contaminants. One way to accomplish this without replacing the current tanks is to fill unused space with removable foam blocks (care is required to avoid creating recesses where contaminants can accumulate and perhaps recontaminate parts). A second way would be to mount new small tanks inside the current tanks.

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Improve flow from inlets to outlets. Inlets and outlets on tanks 4 & 5 are within inches of each other, allowing fresh water to short circuit through the tank. This should be corrected. Most of the tanks have inlets and outlets on opposite sides of the tank at the same level. This is OK, but could be further improved by using plastic hose to feed fresh water to the bottom of the tank so diagonal flow is achieved (an air break would be needed to prevent back siphoning). This could also be used with foam spacers, discussed above, if fresh water feed is distributed over the bottom of the tank or from behind any spacers - flow would be through any cracks or seams and should effectively purge these recesses.

Improve mixing so water currents move high contaminant concentrations away from part. surfaces. This can be accomplished by increasing rinse flow (use cascaded rinses so flows go through all tanks); installing pumps to recirculate rinse water within a tank; or have the carousel lift and descend 5-10 times in each tank. for each step.

C. Check the tubular arms of the carousel for leaks that can carry significant volumes of liquid from tank to tank. The simplest solution is to drill 3/8" holes at the top and bottom of each vertical arm so the arm becomes free draining. Alternatively identify leakers and seal them.

D. Clean scale and solids from tank walls.

Ruldy

also pit in contoct a. Ken Brown

I hope this information is useful, please let me know if I can be of further assistance. Please share this letter with both the supervisor that was so helpful to us and with the cleaning room operators. This information is important to their understanding of the problem, and they may both have other useful information about the water use problem and ideas for solutions.

Sincerely

Karl DeWahl

E. LIST OF RESOURCE PEOPLE

a. Resource People Involved at All Locations

Table V-35 lists the resource people that were involved with the project at all locations. The specific relationship and contact information of each person is cited in the table.

Table	V-35, Contact People for General Information about the Projec	t:
Names	addresses and telephone numbers are included in the table.	In
	addition, a brief relationship to the project is listed.	

Contact	Telephone Number	Address	Relationship to Project
Karl DeWahl	(612)627-1904	MnTAP 1313 5 th St. SE Minneapolis, MN 55414-4504	Intern Advisor
Pat Dick	(612)572-4426	Kurt Manufacturing Company 5280 Main St, NE Minneapolis, MN 55421	general information about water usage and waste generation
Jim Sjoselius	(612)572-4627	Kurt Manufacturing Company 5280 Main St, NE Minneapolis, MN 55421	Intern Supervisor

b. Machining Division and Kurt Gear Division

Contacts listed in Table V-36 are directly related to water conservation at the Machining Division and the Kurt gear Division. The people listed included those involved with the general operation of the Metal Finishing Line and those people involved with any of the implementation process. In addition, contact information for the chemical supplier and is included. The final contact listed provided information about the billing process for both sewer charges and water charges. Table V-36, Contacts Specific to the Machining Division and Kurt Gear Division: People listed include those which can provide general information and those that can provided specific information about implementation and success.

Contact	Telephone	Address	Relationship to
	Number		Project
William Balnchet	(612)378-7581	Industrial Chemical and Equipment 3230 E. Hennepin Ave. Minneapolis, MN 55413	chemical supplier for Metal Finishing Line
Roger Knaus	(612)572-4565	Kurt Manufacturing Company 5280 Main St, NE Minneapolis, MN 55421	Metal Finishing Line operator (day shift)
Judy Melham	(612)572-3529	City of Fridley	water charges and sewer charges information
Marty Meyer	(612)926-6713	UNIFAB, Inc. 3850 Edgewood Ave. St. Louis Park, MN 55426	polypropylene tank construction
Dave Muncy	(612)572-1500	Kurt Manufacturing Company 5280 Main St, NE Minneapolis, MN 55421	Metal Finishing Line operator (night shift)
Bruce Powers	(612)572-4419	Kurt Manufacturing Company 5280 Main St, NE Minneapolis, MN 55421	Maintenance Supervisor
Chris Wiege	(612)427-4940	Climatronics, HVAC/R 11833 Douglas Dr. N. Minneapolis, MN 55316	plumbing and weir construction

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c. Resource People Involved at the Automatic Division

Table V-37 lists the resource people that were involved with the project at the Automatic Division.

Table V-37, Contact People for Information about the Project at the Automatic Division:

Names addresses and telephone numbers are included in the table. In addition, a brief relationship to the project is listed.

Contact	Telephone	Address	Relationship to
	Number	·	Project
Laura Engen	(612)602-4712	Metropolitan Council	SAC information
		Environmental Services	
		Mears Park Centre	
		230 E 5 th St.	
		St. Paul, MN	
		55101-1633	
Mike Frantz	(612)572-4549	Kurt Manufacturing	Maintenance
ala na sa		Company	Department
		1292 Northdale Blvd.	
		Coon Rapids, MN	
		55448	ана така Стала 19
Tom Loeschke	(612)572-4488	Kurt Manufacturing	Quality
·		Company	Supervisor
		1292 Northdale Blvd.	
		Coon Rapids, MN	
		55448	

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